

Model Order Reduction and Bayesian Optimization for MDO problems

ines.cardoso@onera.fr

Inês CARDOSO^{a,b} – Gaspard BERTHELIN^{a,b} – Sylvain DUBREUIL^a – Michel SALAÜN^b – Nathalie BARTOLI^a – Christian GOGU^b

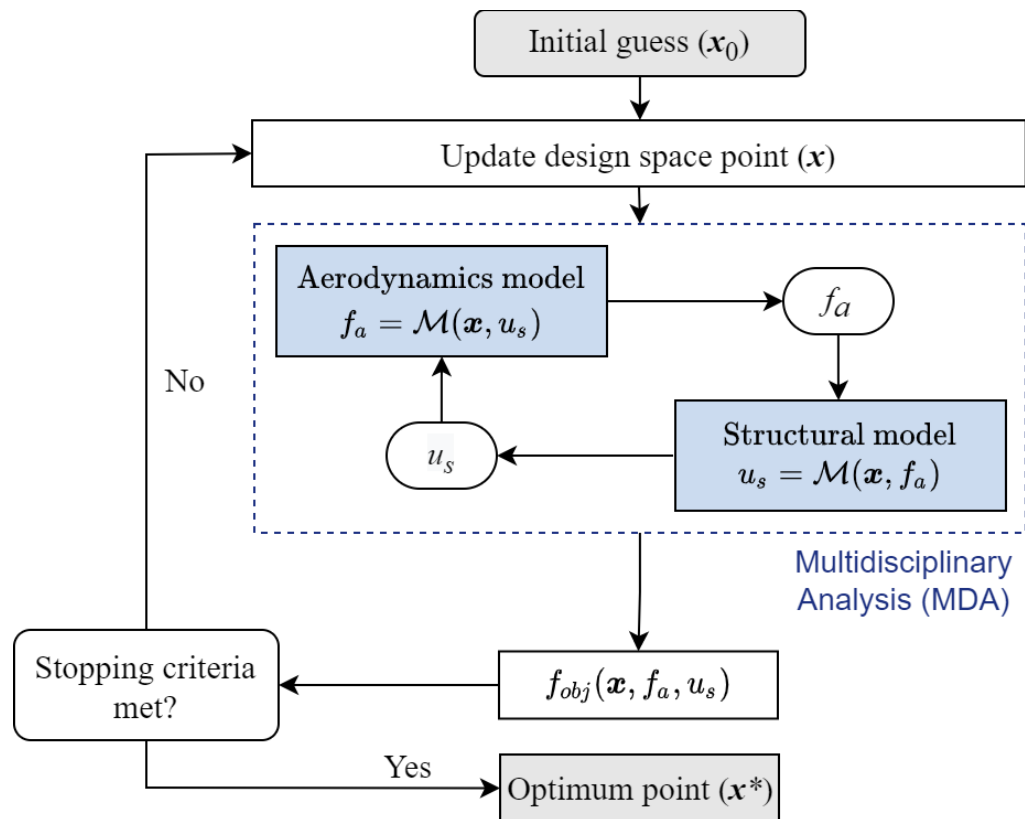
a. DTIS, ONERA, Université de Toulouse, Toulouse France

b. Université de Toulouse, CNRS, UPS, INSA, ISAE, Mines Albi, Institut Clément Ader (ICA), Toulouse, France

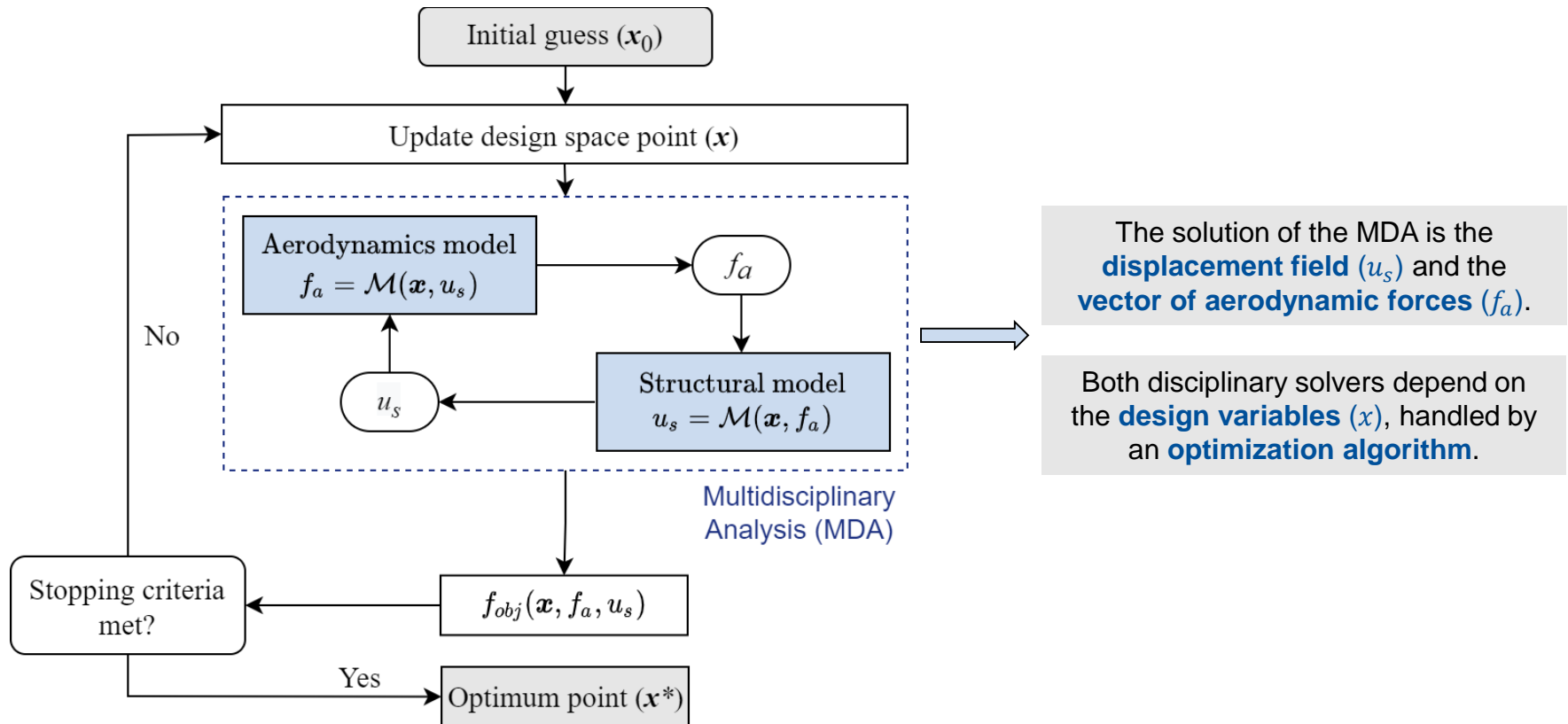
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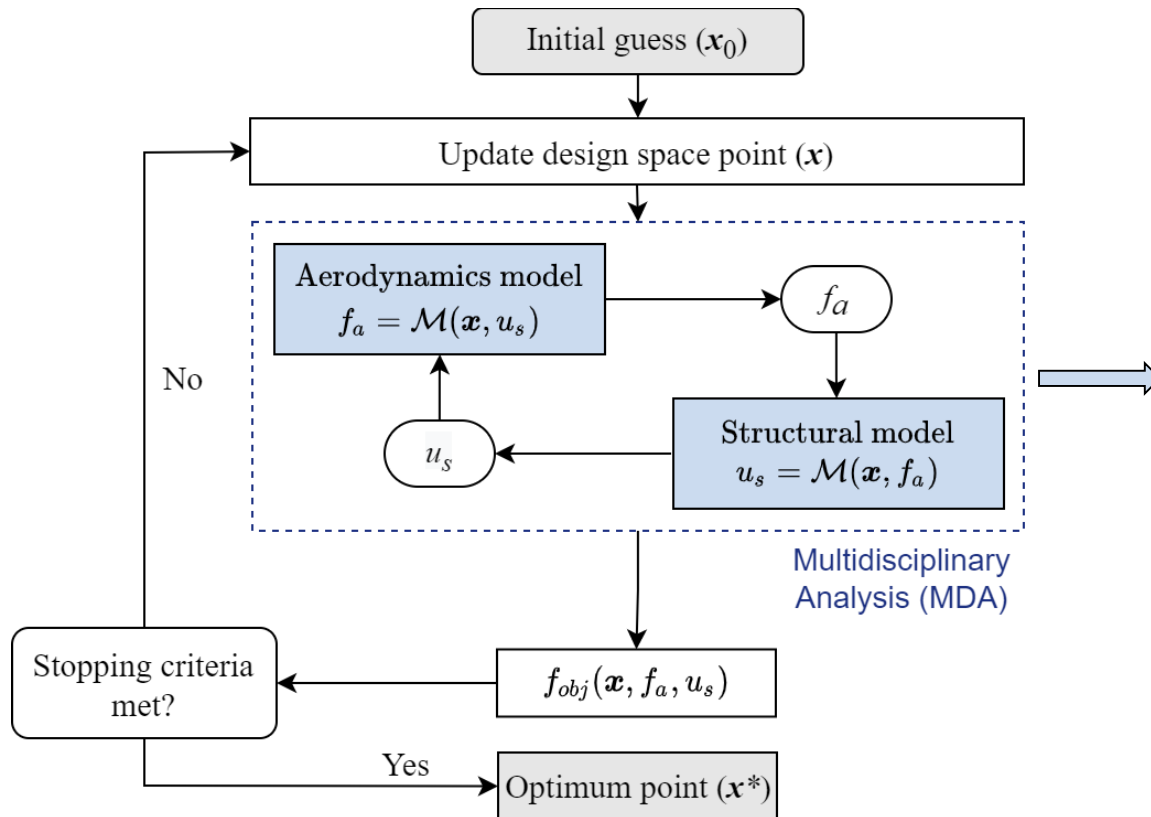
Static aeroelastic optimization of an aircraft wing



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The solution of the MDA is the **displacement field** (u_s) and the **vector of aerodynamic forces** (f_a).

Both disciplinary solvers depend on the **design variables** (x), handled by an **optimization algorithm**.

Assumptions:

- Partitioned approach: **non-intrusive coupling** between the disciplinary solvers.
- Multidisciplinary Feasible (MDF) approach: optimization problem and non-linear coupled problem **solved independently**.
- The coupling variables are **high dimensional** vectors.

Problem statement

Problem:

- When using high fidelity solvers (e.g. FEM or CFD solvers), the **computational cost** may become intractable.

Goal:

- Reduce the computational cost, by **reducing the number of disciplinary solver calls** made.

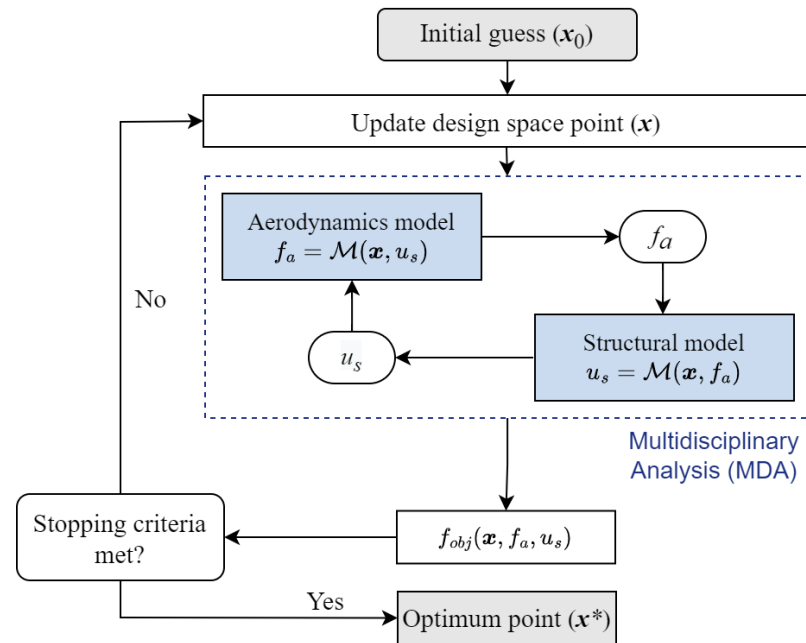
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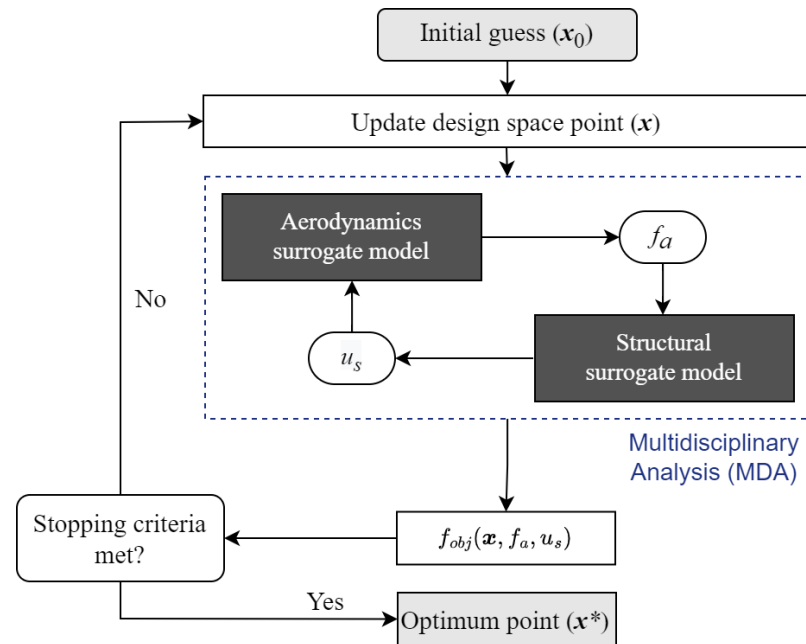
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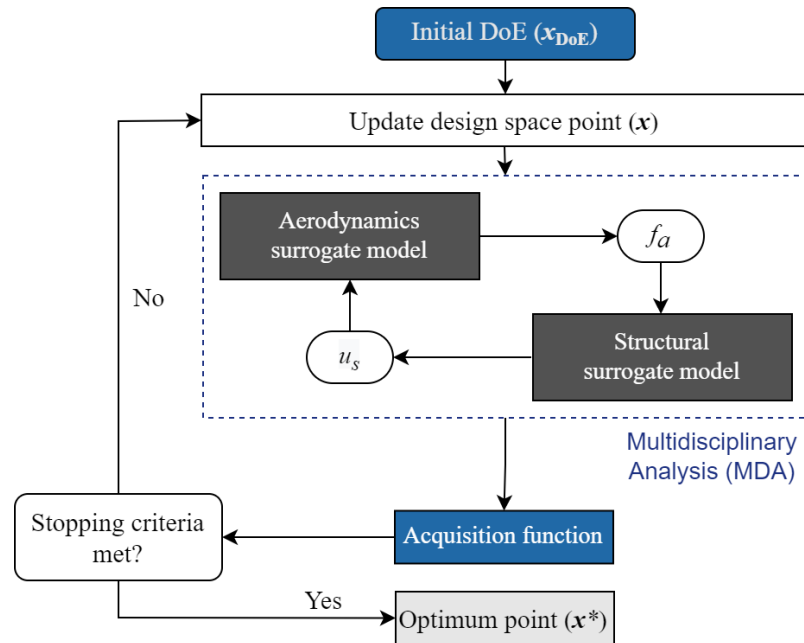
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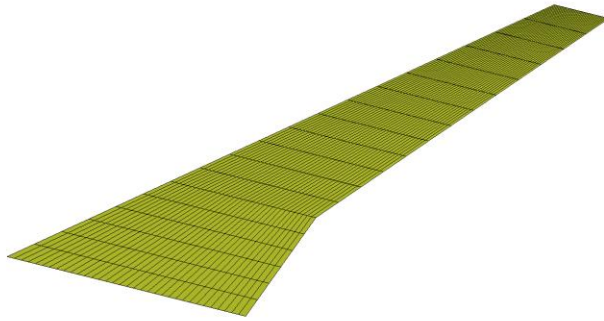


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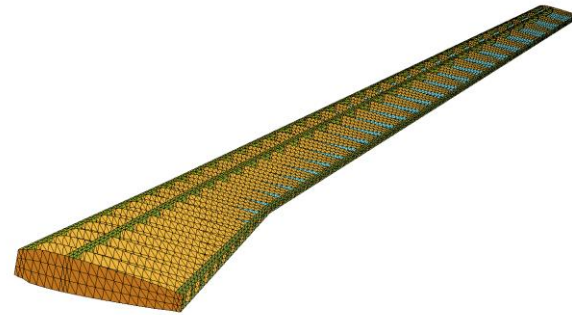
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Aerodynamics and Structural solvers

➤ Common Research Model (configuration uCRM-9) [1]:



Aerodynamics mesh (VLM solver – 2100 degrees of freedom)

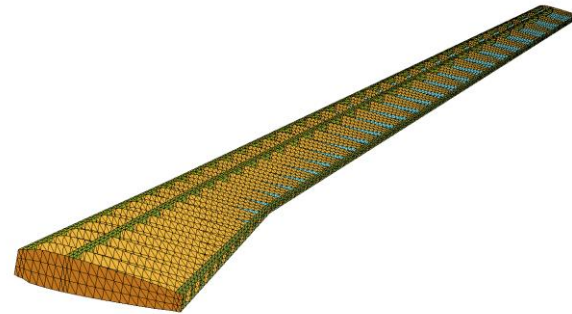
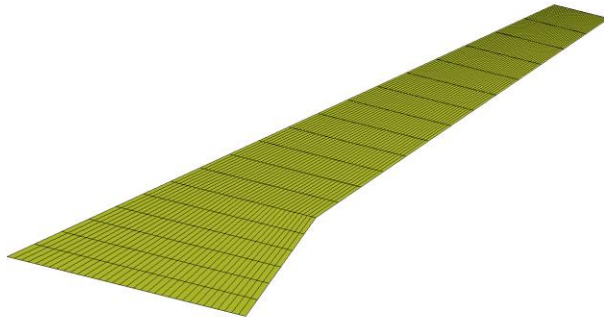


Structural mesh (FEM solver – 43416 degrees of freedom)

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Aerodynamics and Structural solvers

- **Common Research Model (configuration uCRM-9) [1]:**



Aerodynamics mesh (VLM solver – 2100 degrees of freedom)

Structural mesh (FEM solver – 43416 degrees of freedom)

- Four considered **design variables** ($\mathbf{x} = \{\alpha, V_\infty, t_{sk}, t_{sp}\}$):

Variable	$\alpha [^\circ]$	$V_\infty [m/s]$	$t_{sk} [m]$	$t_{sp} [m]$
Designation	Angle of attack	Air freestream velocity	Skin thickness	Spar thickness
Range of variation	[1, 9]	[220, 250]	[0.003, 0.01]	[0.01, 0.1]

The design variables were scaled to take values in the range [0,1].

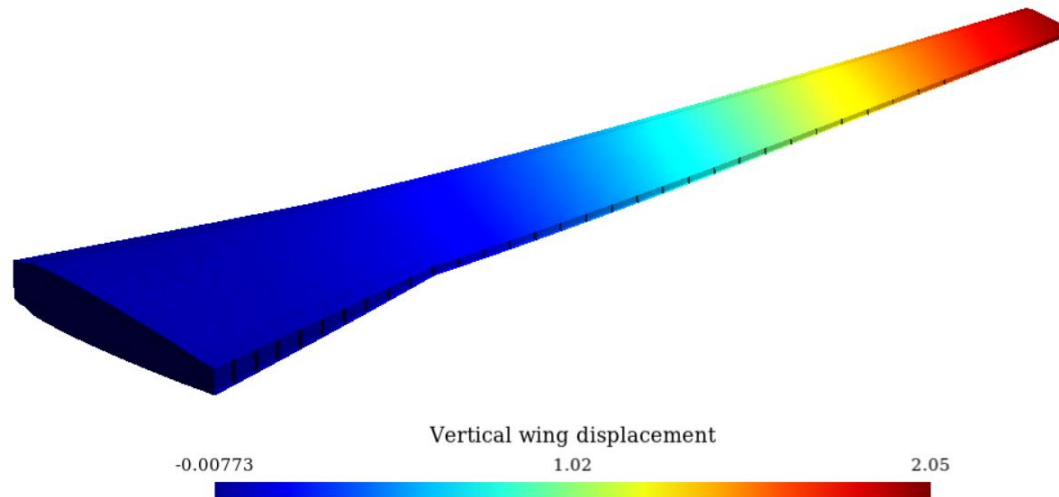
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Objective function

- Objective function chosen as an **inverse problem**:

$$\mathbf{x}^* = \arg \min_{\mathbf{x} \in \mathcal{X}} f_{obj}(\mathbf{x}) \quad \text{with} \quad f_{obj}(\mathbf{x}) = \frac{\|f_a(\mathbf{x}_{ref}) - f_a(\mathbf{x})\|_2}{\|f_a(\mathbf{x}_{ref})\|_2} + \frac{\|u_s(\mathbf{x}_{ref}) - u_s(\mathbf{x})\|_2}{\|u_s(\mathbf{x}_{ref})\|_2}$$

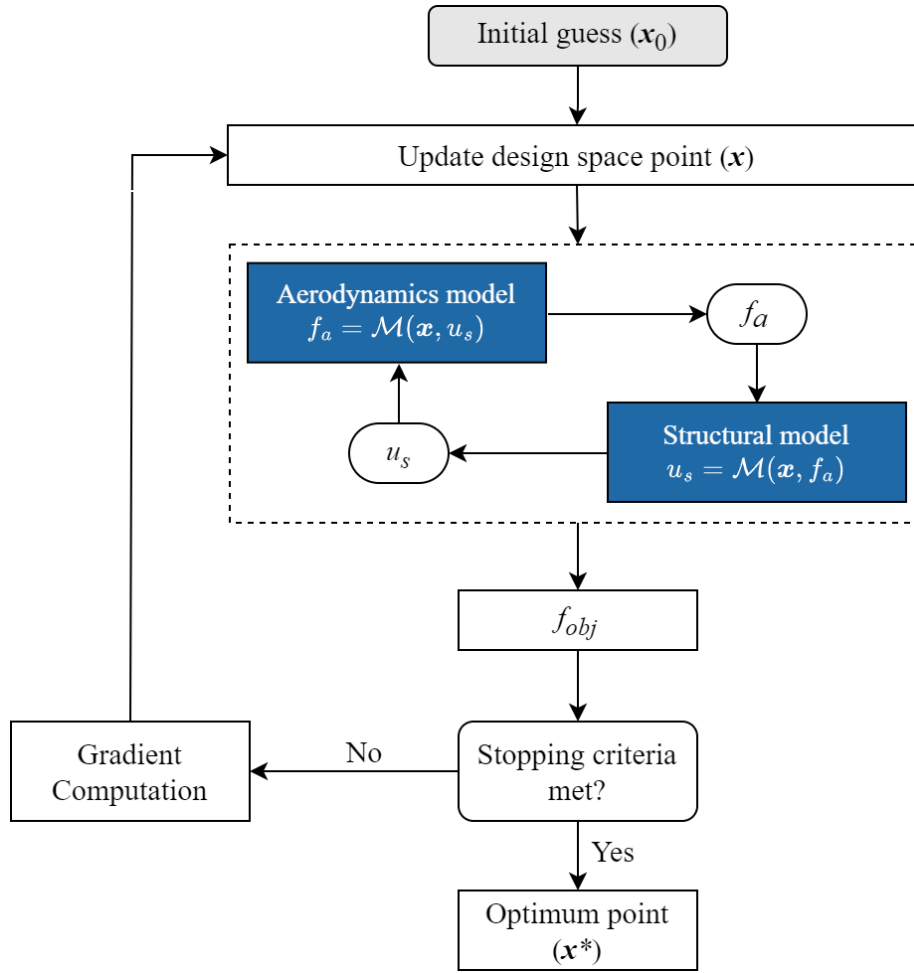
with \mathbf{x}_{ref} the design space point that results in the **maximum wing tip displacement** $\mathbf{x}_{ref} = \{1,1,0,0\}$.



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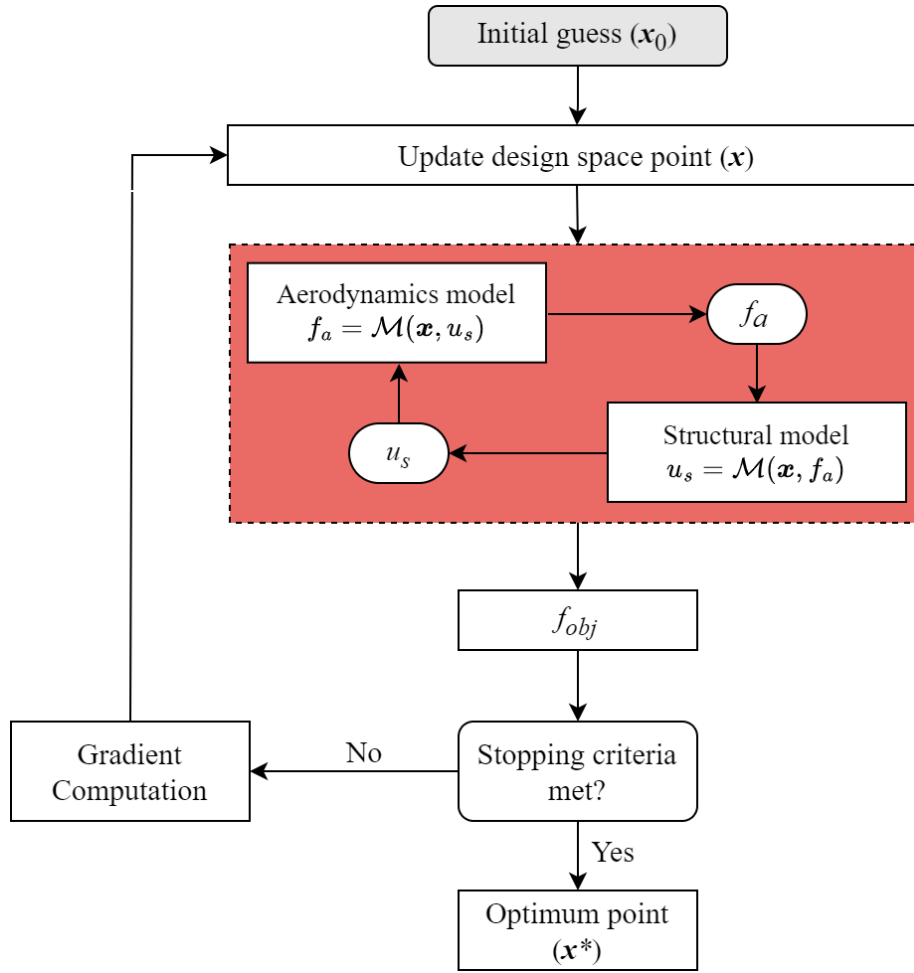
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Reference optimization framework



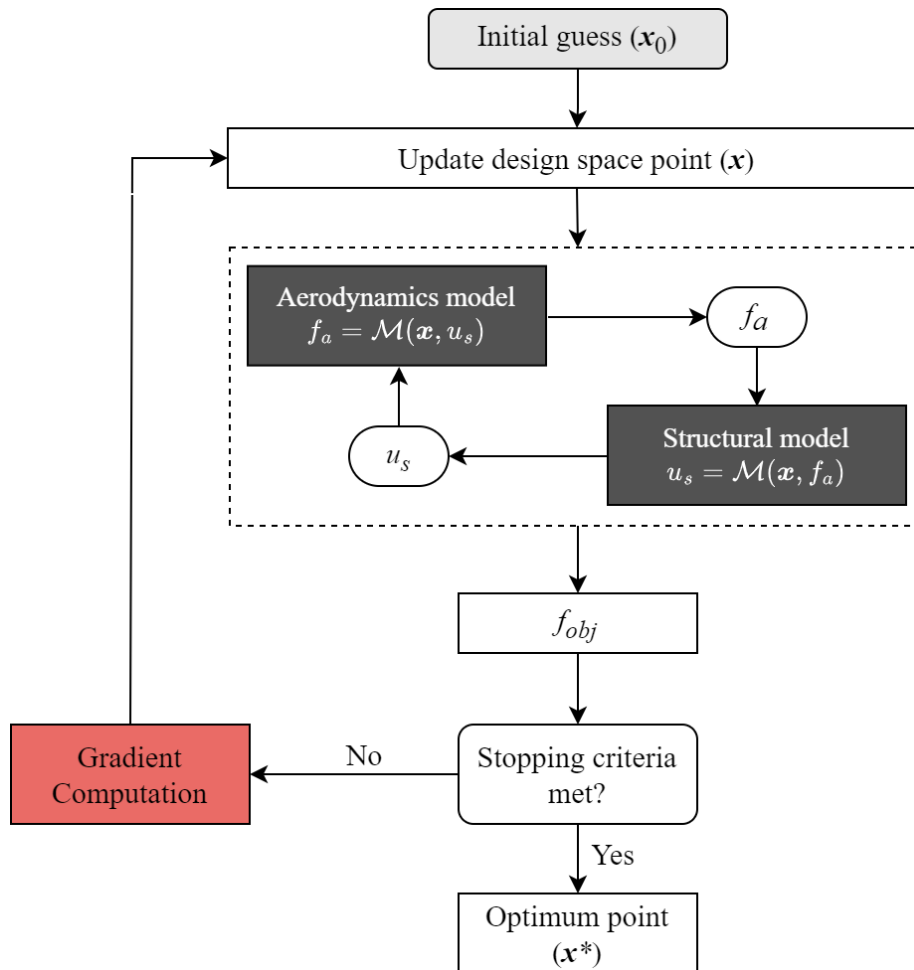
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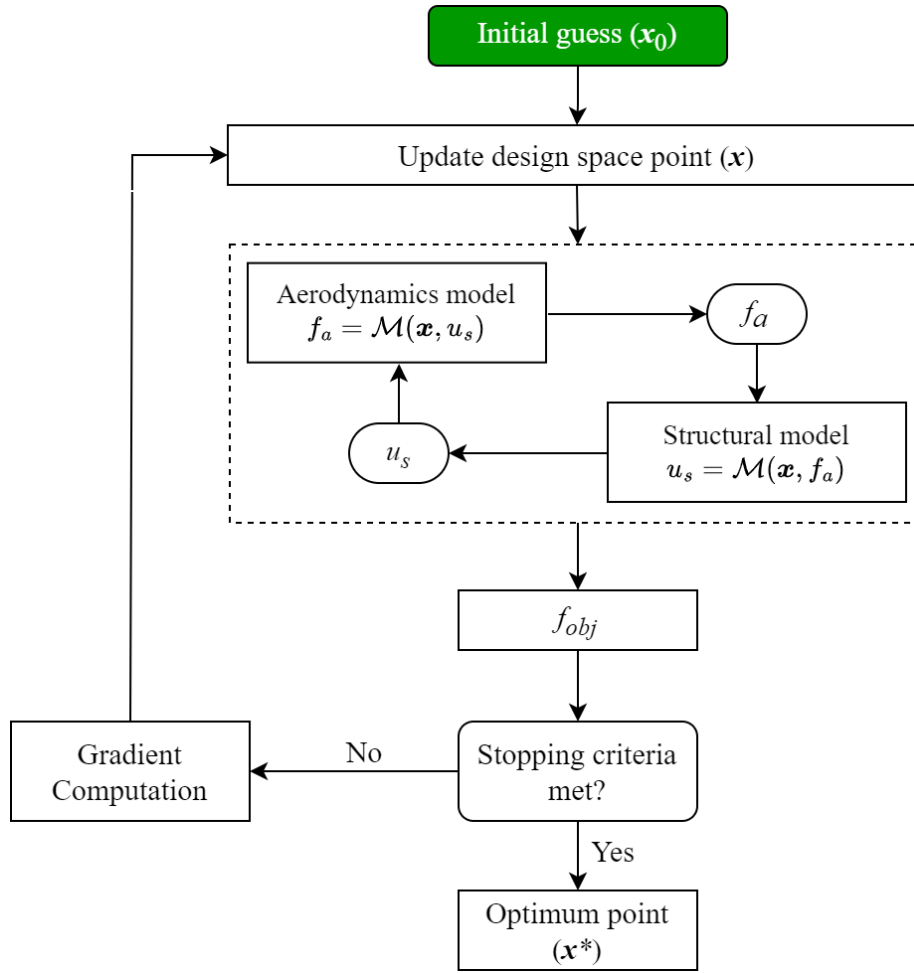
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⇒ **MDA is solved at every iteration.**

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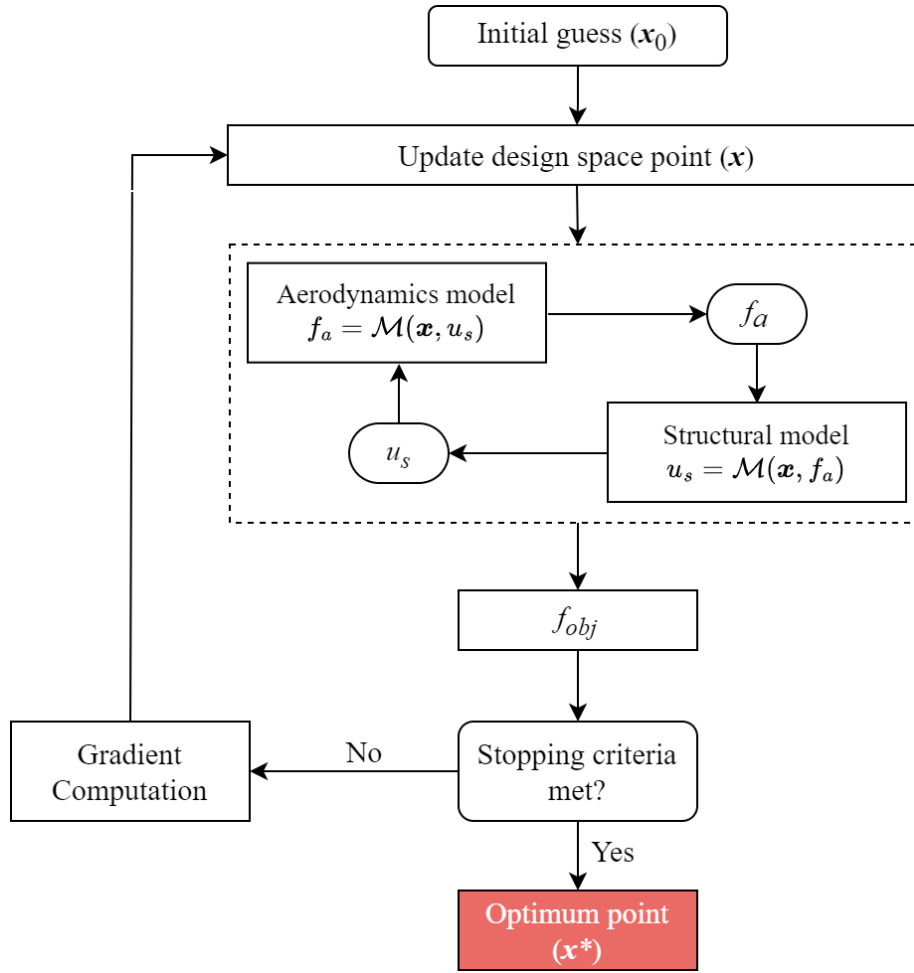
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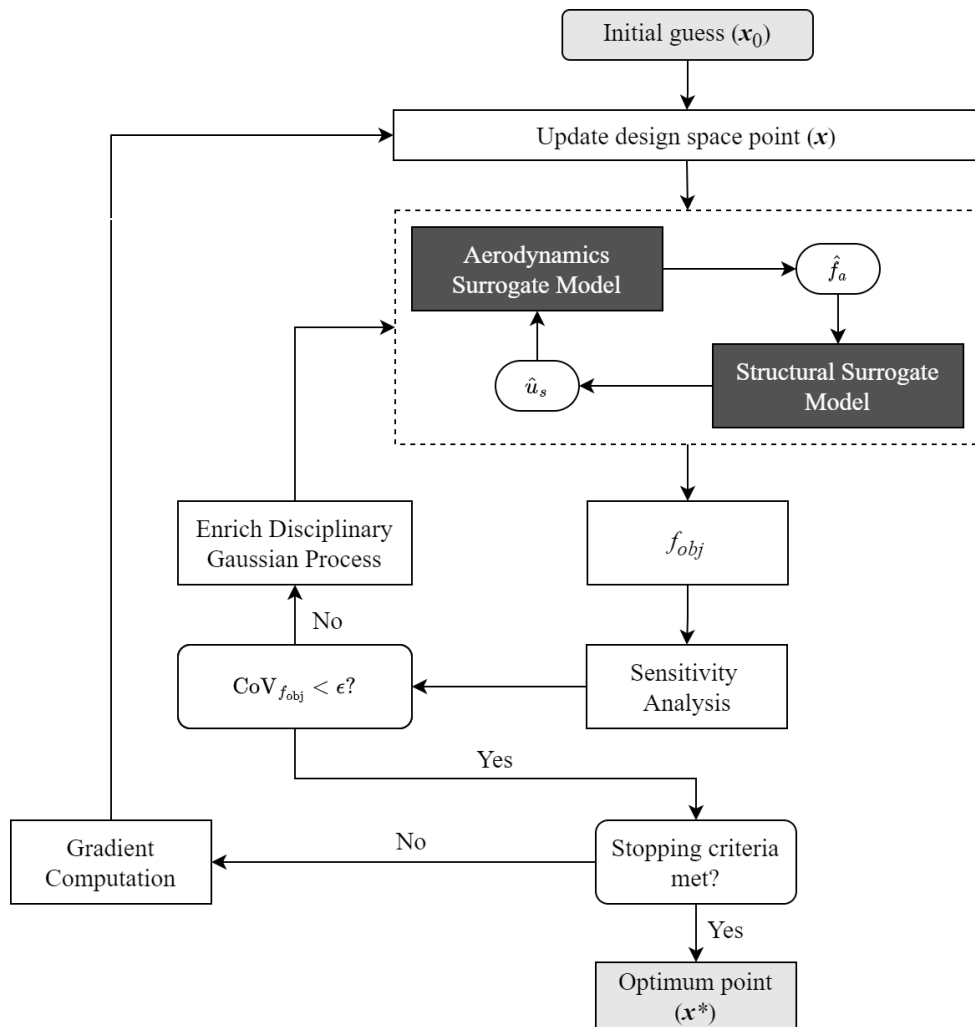


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 - Starting point chosen at the center of the design space $x_0 = \{0.5, 0.5, 0.5, 0.5\}$.
- ⇒ The algorithm needed 17 iterations and **286 calls** to each disciplinary solver in order to find the reference point.

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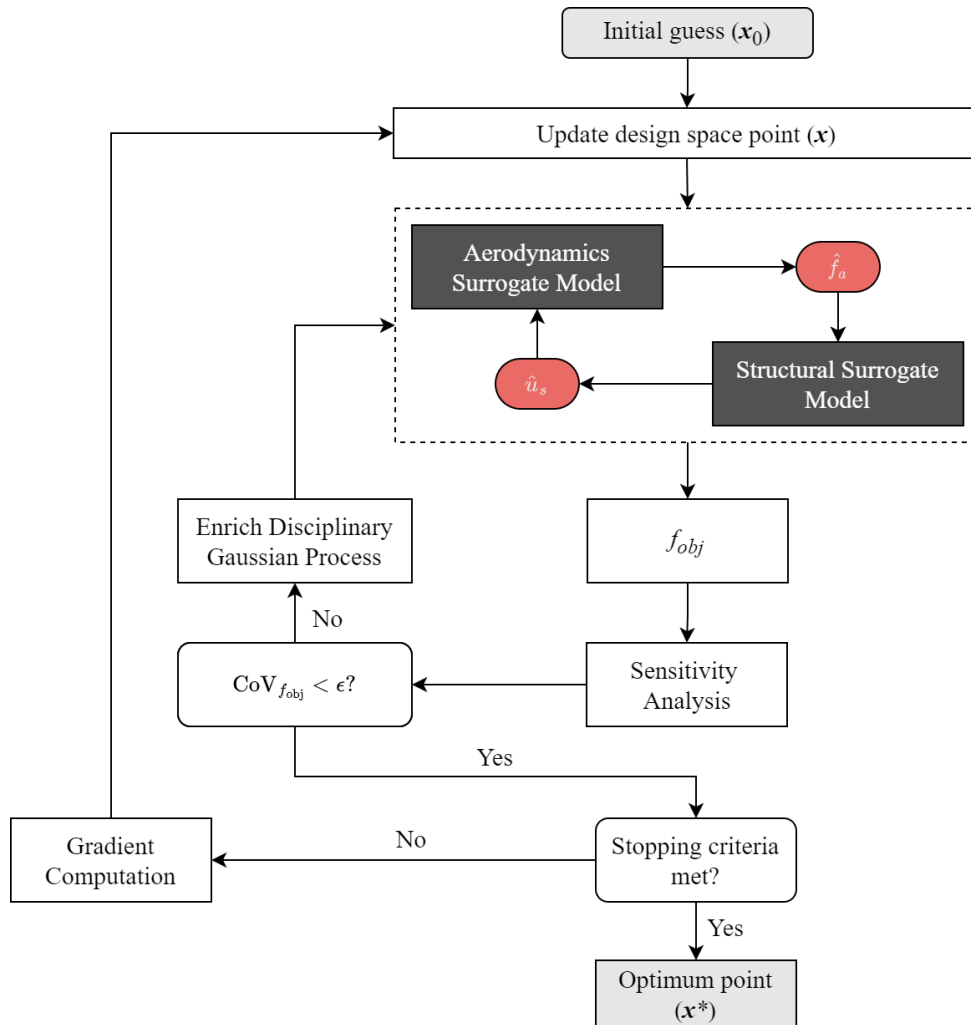
DPOD+I & SLSQP framework



- Replacement of the disciplinary solvers by **Disciplinary Proper Orthogonal Decomposition + Interpolation (DPOD+I) surrogate models [2]**.

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⇒ Model order reduction by **Disciplinary Proper Orthogonal Decomposition (DPOD)**:

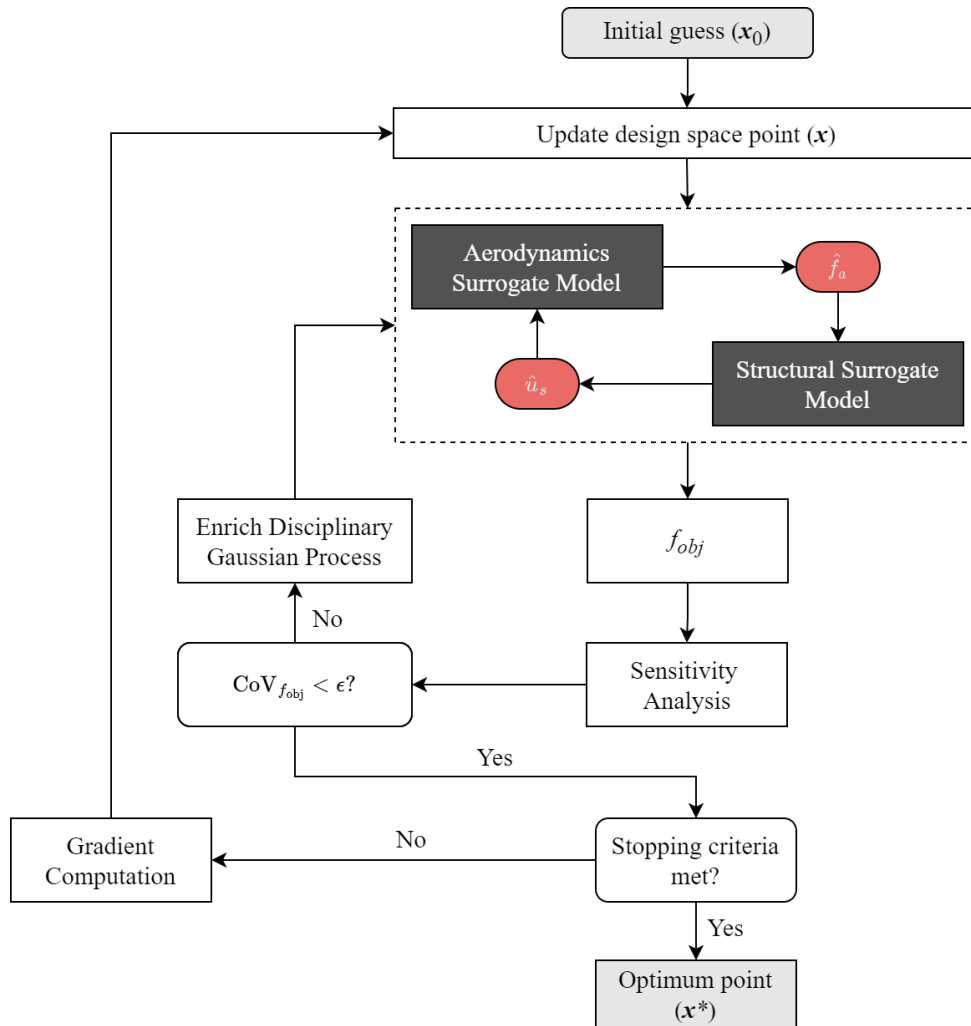
$$\hat{f}_a \approx \phi_0^a + \sum_{i=1}^{n_a} \alpha_i^a(\mathbf{x}, u_s) \phi_i^a$$

$$\hat{u}_s \approx \phi_0^s + \sum_{i=1}^{n_s} \alpha_i^s(\mathbf{x}, f_a) \phi_i^s$$

where ϕ_0 is a constant vector, ϕ_i are the POD basis vectors, α_i are the POD coefficients, and n_a and n_s give the number of terms retained in the POD approximations.

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- Replacement of the disciplinary solvers by **Disciplinary Proper Orthogonal Decomposition + Interpolation (DPOD+I)** surrogate models [2].

⇒ Model order reduction by **Disciplinary Proper Orthogonal Decomposition (DPOD)** followed by the interpolation of each coefficient by **Gaussian Processes (GP)**:

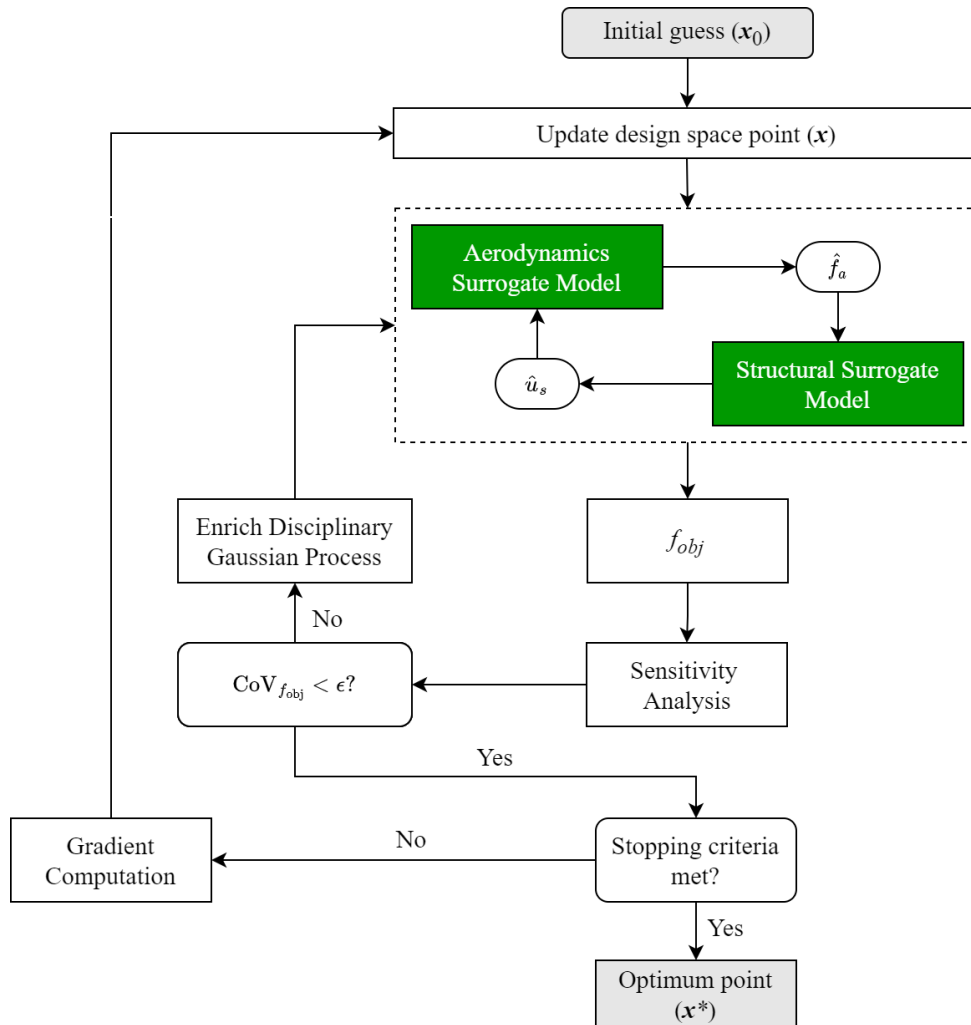
$$\hat{\alpha}_i^a \sim \text{GP} |_{\text{DoE}_a} (\mu |_{\text{DoE}_a}, k |_{\text{DoE}_a})$$

$$\hat{\alpha}^s \sim \text{GP} |_{\text{DoE}_s} (\mu |_{\text{DoE}_s}, k |_{\text{DoE}_s})$$

where the GP approximation of the coefficients is denoted by $\hat{\alpha}_i$ and is characterized by a mean value μ and a covariance kernel k .

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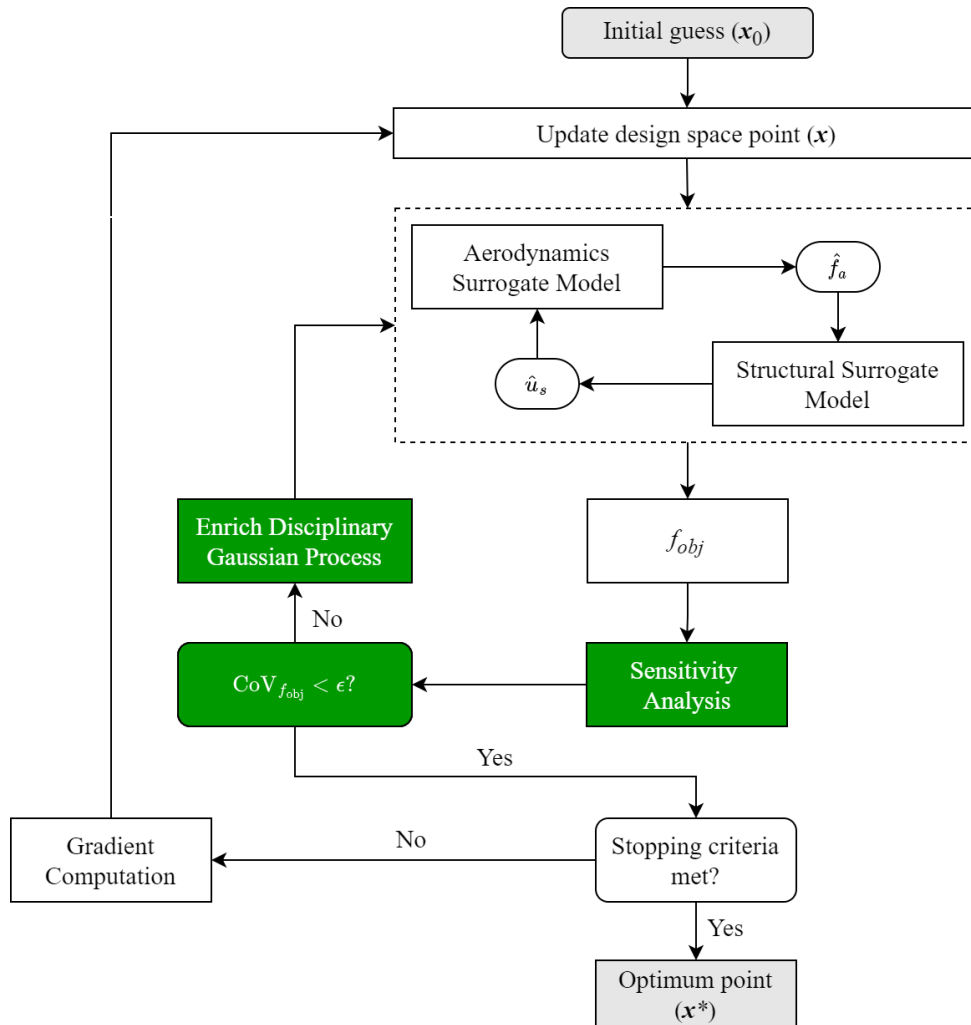


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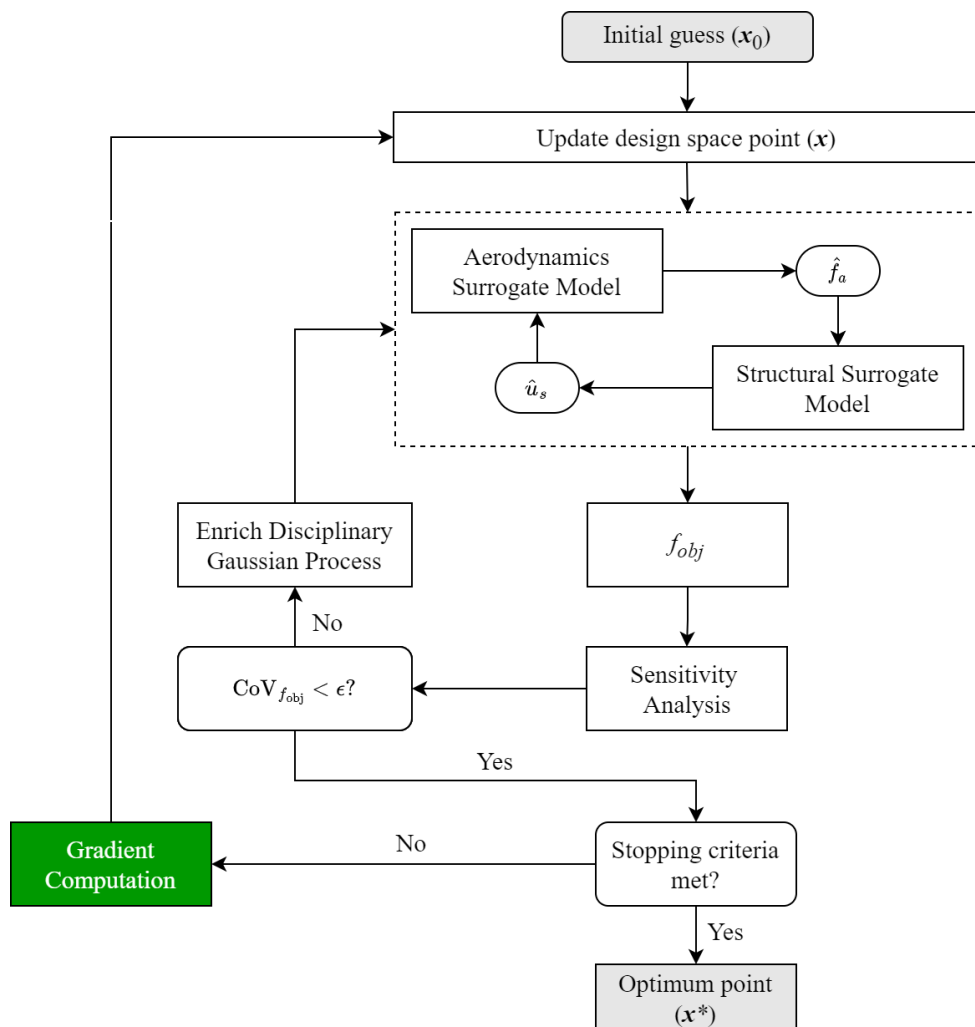
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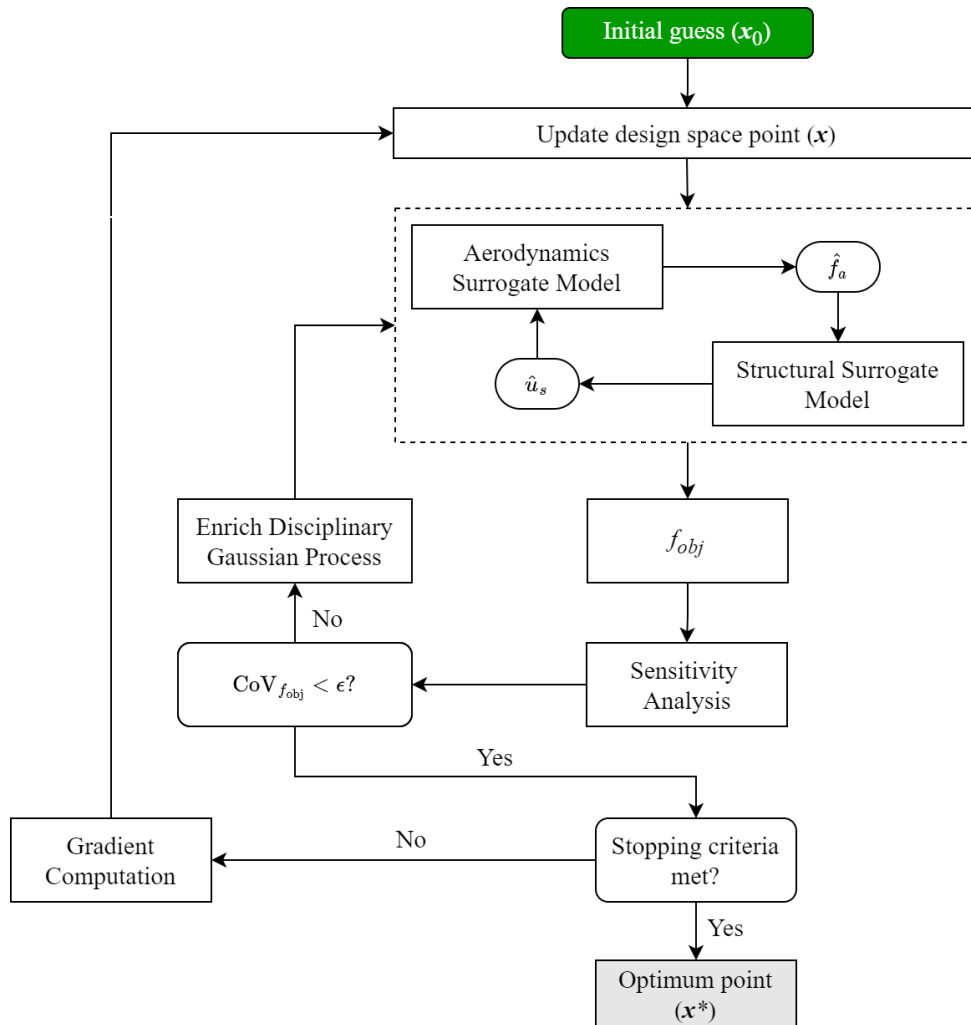
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- Structural POD basis composed of an average of 6 coefficients and aerodynamics POD basis composed of an average of 5 coefficients.

 \Rightarrow **Initial DoE:** average of 42 points for the structural discipline and 52 for the aerodynamics discipline.

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Comparison between DPOD+I & SLSQP framework and reference framework

		α^*	V_∞^*	t_{sk}^*	t_{sp}^*	$f(\mathbf{x}^*)$	n^a	n^s
Reference	\mathbb{E}	1.0	1.0	0.0	0.0	0.0	286	286
	CoV	—	—	—	—	—	—	—
DPOD+I & SLSQP	\mathbb{E}	1.0	1.0	3.4×10^{-4}	3.1×10^{-4}	0.0585	60.7	51.5
	CoV	$\leq 10^{-12}$	$\leq 10^{-12}$	3.0	2.6346	0.1523	0.1904	0.1784

where n^a and n^s are, respectively, the number of aerodynamics solver calls and the number of structural solver calls.

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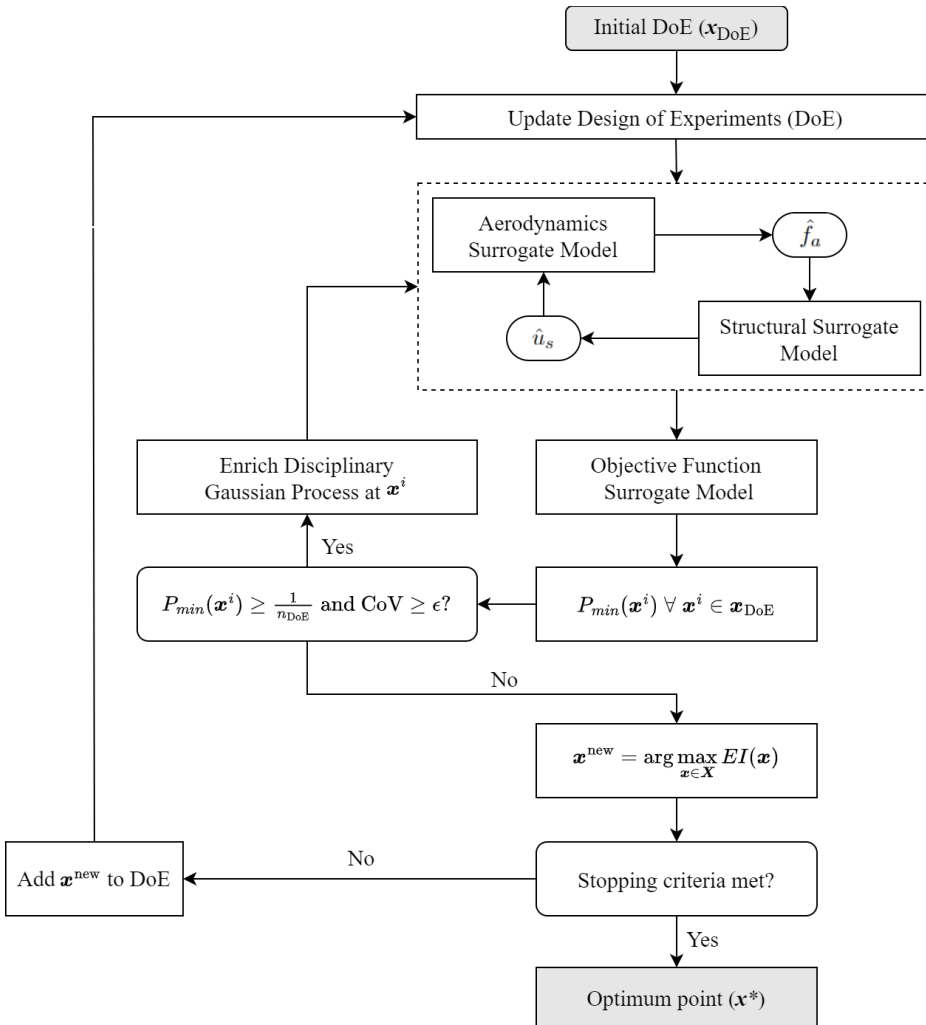
where n^a and n^s are, respectively, the number of aerodynamics solver calls and the number of structural solver calls.

- \Rightarrow **Reduction by a factor of 5** in the number of necessary disciplinary solver calls.
- \Rightarrow An average of **only 10 calls** was made to each disciplinary solver during the optimization process.

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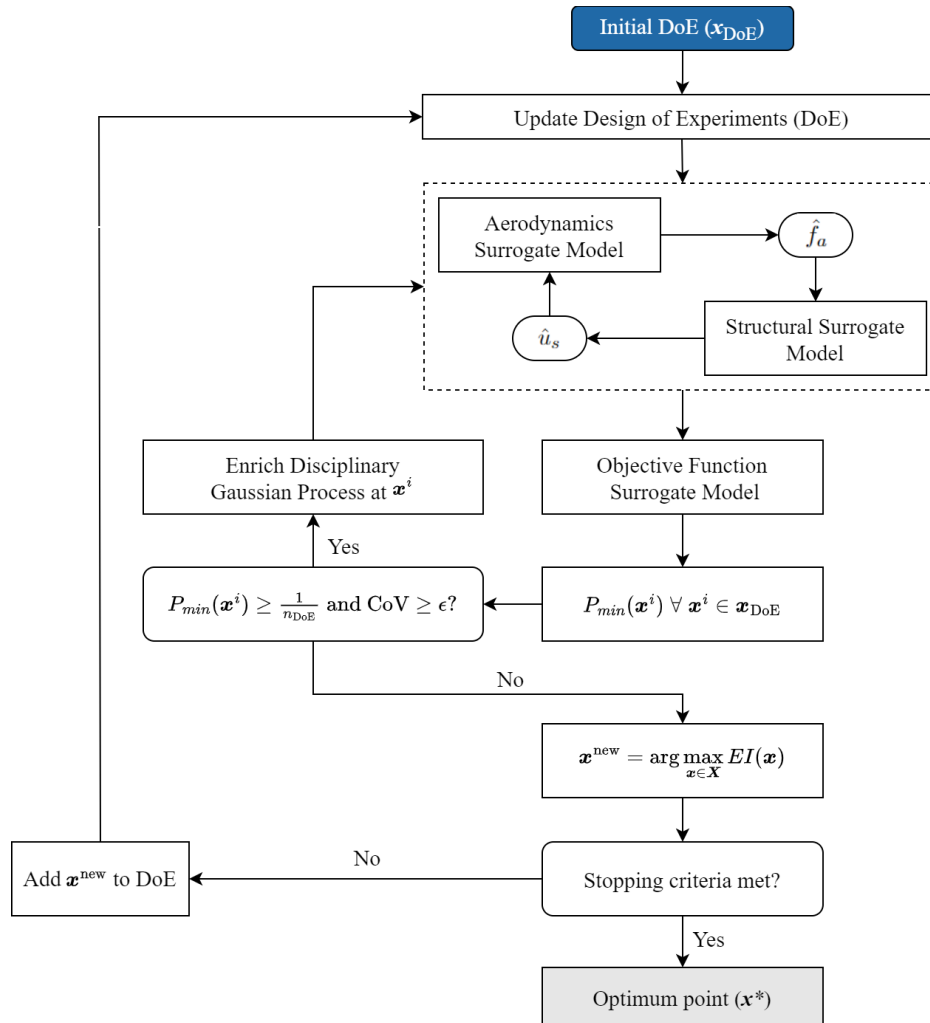
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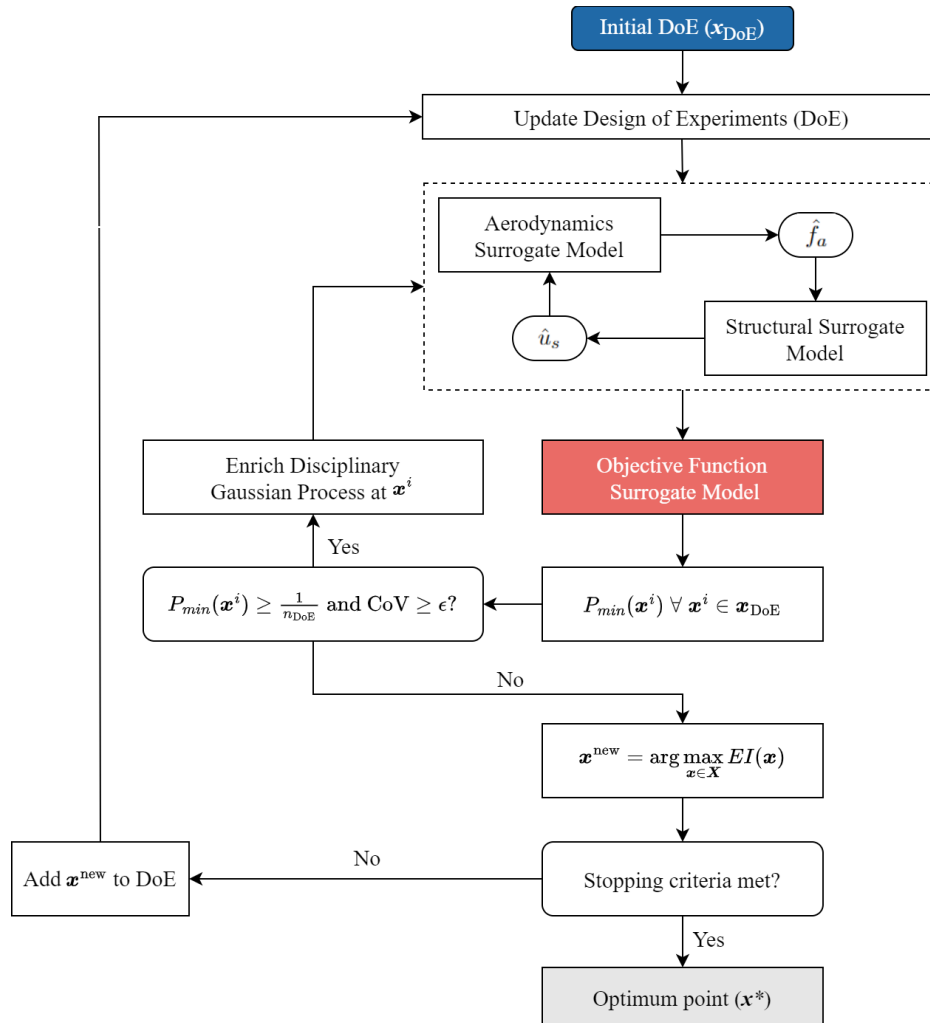
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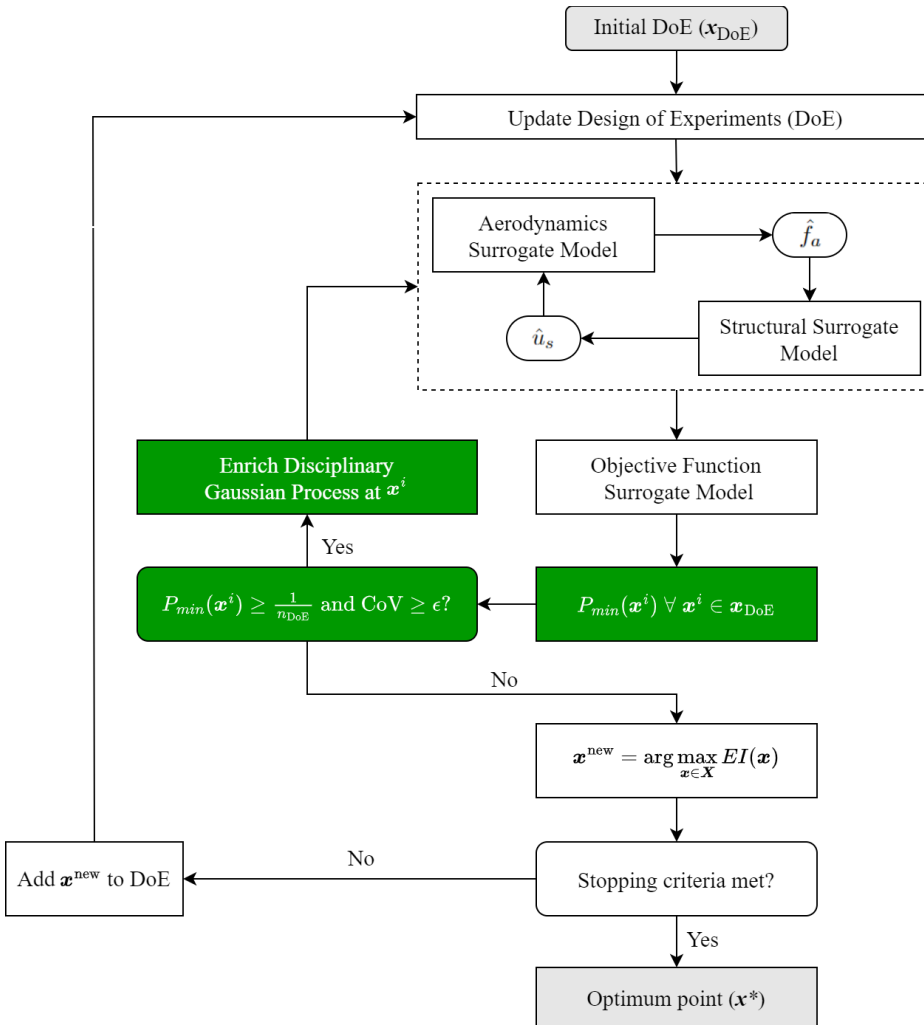
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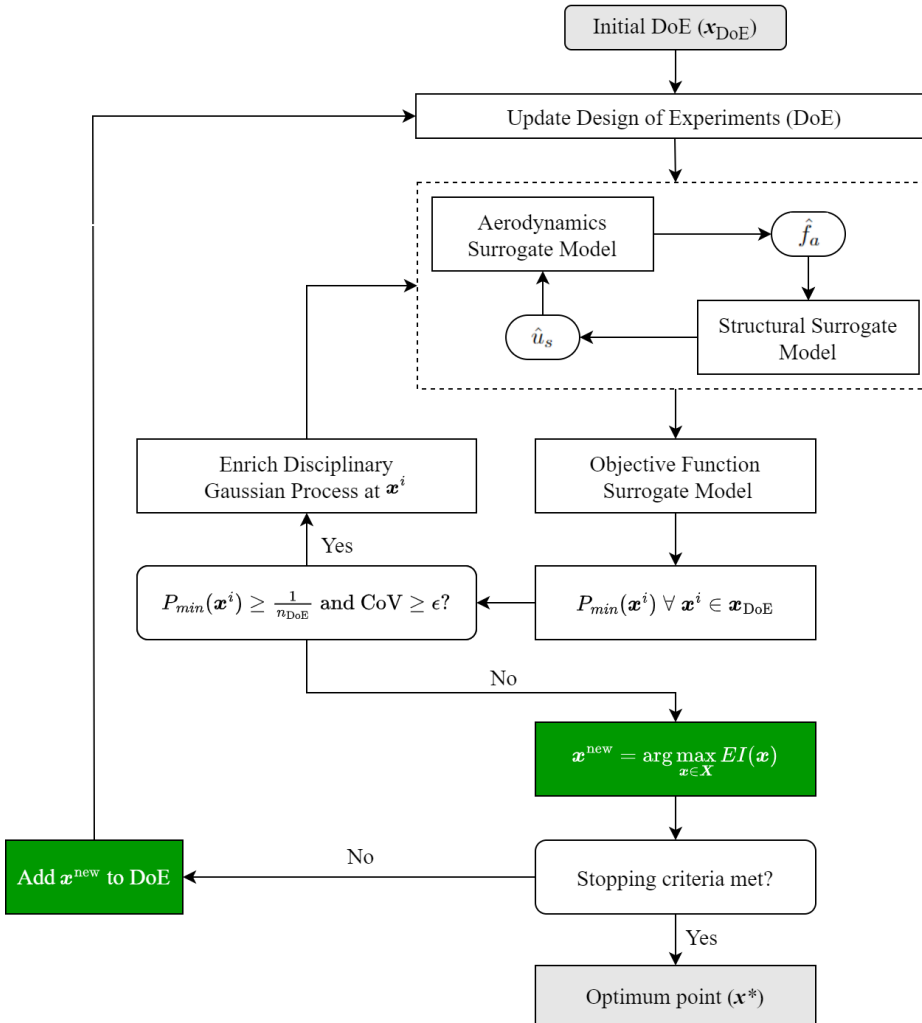
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- It remains possible to enrich the disciplinary surrogate models at DoE points.
- ✓ The point must have some **likelihood of being the minimum** to be enriched.

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- ✓ The point must have some **likelihood of being the minimum** to be enriched.
- Possible to add new points to the DoE.
- ✓ A modified **Expected Improvement (EI)** criterion is used.
 - ⇒ Due to the non-Gaussian nature of f_{obj} the **EI is estimated via Monte Carlo Simulation**.

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DPOD+I & EGMDO	\mathbb{E}	0.999	0.987	0.006	3×10^{-7}	0.044	61	51
	CoV	0.003	0.02	0.9	3.16	0.44	0.1117	0.1225

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DPOD+I & EGMDO	\mathbb{E}	0.999	0.987	0.006	3×10^{-7}	0.044	61	51
	CoV	0.003	0.02	0.9	3.16	0.44	0.1117	0.1225

where n^a and n^s are, respectively, the number of aerodynamics solver calls and the number of structural solver calls.

- **Reduction by a factor of 5** on the number of necessary disciplinary solver calls compared to the reference framework.

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Conclusion and perspectives

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- Some perspectives to the proposed framework include the implementation of **other dimension reduction techniques**, for instance via local POD basis or non-linear model order reduction, to account for more complex disciplinary models. **Other approximation models**, such as the Kriging with Partial Least Squares model [4] could allow the construction of GPs for a greater number of design variables.

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