

# Benchmark reliability problems - A selected list

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# 1 Example 1

Source: Bourinet (2018, Appendix A, Example 2)

Random inputs:  $U_1, U_2 \sim \mathcal{N}(0, 1), U_1$  and  $U_2$  independent.

Limit-state function:

$$G(\mathbf{u}) = \min_{k \in \{1,2\}} G_k(\mathbf{u}) \text{ for } \mathbf{u} = (u_1, u_2)^{\mathrm{T}},$$

where

$$G_{1}(\mathbf{u}) = (u_{1} - \epsilon) + \beta_{1},$$

$$G_{2}(\mathbf{u}) = \beta_{1} \left( 1 - \left[ \frac{1}{2} \left( \frac{u_{1} - \epsilon}{\beta_{2}} + \left| \frac{u_{1} - \epsilon}{\beta_{2}} \right| \right) \right]^{\gamma} \right),$$

and where  $\beta_1 = 6$ ,  $\beta_2 = 4.5$ ,  $\gamma = 30$ ,  $\epsilon = 10^{-6}$ .

Reference failure probability:  $p_{\text{fref}} = \Phi(-(\beta_1 - \epsilon)) + \Phi(-(\beta_2 + \epsilon)) \approx \Phi(-\beta_2) = 3.40 \times 10^{-6}$ .

## 2 Example 2

Source: Bjerager (1988), Engelund and Rackwitz (1993), and Bourinet (2016)

Random inputs:  $U_1, \ldots, U_5 \sim \mathcal{N}(0, 1), U_1, \ldots, U_5$  independent.

Limit-state function:

$$G(\mathbf{u}) = \max_{k \in \{1,4\}} G_k(\mathbf{u}) \text{ for } \mathbf{u} = (u_1, \dots, u_5)^{\mathrm{T}},$$

where

$$G_1(\mathbf{u}) = 2.677 - u_1 - u_2,$$
  

$$G_2(\mathbf{u}) = 2.500 - u_2 - u_3,$$
  

$$G_3(\mathbf{u}) = 2.323 - u_3 - u_4,$$
  

$$G_4(\mathbf{u}) = 2.250 - u_4 - u_5.$$

Reference failure probability:  $p_{\text{fref}} = \Phi_4(-\beta, 0, \mathbf{R}) = 2.13 \times 10^{-4}$  where  $\beta$  is the vector of HL reliability indices, **R** is the correlation matrix between the four limit-state surfaces and  $\Phi_4$  is the 4-dimensional normal CDF.

#### 3 Example 3

Source: De Stefano and Der Kiureghian (1990) and Bourinet et al. (2011)

Random inputs: The 8 random inputs are independent. The marginal PDFs are defined in Table 1.

Variable	$m_{\rm p}$	$m_{\rm s}$	$k_{ m p}$	$k_{ m s}$	$\zeta_{ m p}$	$\zeta_{\rm s}$	$F_{s}$	$S_0$
Distribution				logne	ormal			
Mean	1.5	0.01	1	0.01	0.05	0.02	27.5	100
C.o.V.	0.1	0.1	0.2	0.2	0.4	0.5	0.1	0.1

Table 1 – Example 3 - Random inputs.

Limit-state function:

$$g(\mathbf{x}) = F_{\rm s} - 3k_{\rm s} \sqrt{\frac{\pi S_0}{4\zeta_{\rm s}\omega_{\rm s}^3}} \left[ \frac{\zeta_{\rm a}\zeta_{\rm s}}{\zeta_{\rm p}\zeta_{\rm s} (4\zeta_{\rm a}^2 + \theta^2) + \gamma \zeta_{\rm a}^2} \frac{\left(\zeta_{\rm p}\omega_{\rm p}^3 + \zeta_{\rm s}\omega_{\rm s}^3\right)\omega_{\rm p}}{4\zeta_{\rm a}\omega_{\rm a}^4} \right]$$

where  $\mathbf{x} = (m_{\rm p}, m_{\rm s}, k_{\rm p}, k_{\rm s}, \zeta_{\rm p}, \zeta_{\rm s}, F_{\rm s}, S_0)^{\rm T}$ , and where  $\omega_{\rm p} = \sqrt{k_{\rm p}/m_{\rm p}}$ ,  $\omega_{\rm s} = \sqrt{k_{\rm s}/m_{\rm s}}$ ,  $\omega_{\rm a} = (\omega_{\rm p} + \omega_{\rm s})/2$ ,  $\zeta_{\rm a} = (\zeta_{\rm p} + \zeta_{\rm s})/2$ ,  $\gamma = m_{\rm s}/m_{\rm p}$  and  $\theta = (\omega_{\rm p} - \omega_{\rm s})/\omega_{\rm a}$ .

Reference failure probability:  $p_{\rm fref} = 3.78 \times 10^{-7}$ .

## 4 Example 4

Source: Kouassi et al. (2016), Bourinet (2018, Appendix A, Example 1), Bourinet (2019)

Random inputs: The 11 random inputs are independent. The marginal PDFs are defined in Table 2.

variable X <sub>i</sub>	mean $\mu_{X_i}$ c.o.v. $\delta_{X_i}$		distribution / support		
$\overline{X_1 = L \ (\mathbf{m})}$	4.2	0.10	lognormal / $\mathbb{R}_{\geq 0}$		
$X_2 = h$ (m)	0.02	0.10	lognormal / $\mathbb{R}_{\geq 0}$		
$X_3 = d$ (m)	0.001	0.05	lognormal / $\mathbb{R}_{\geq 0}$		
$X_4 = Z_L (\Omega)$	1000	0.20	lognormal / $\mathbb{R}_{\geq 0}$		
$X_5 = Z_0 \ (\Omega)$	50	0.05	lognormal / $\mathbb{R}_{\geq 0}$		
$X_6 = a_e \text{ (V/m)}$	1	0.20	lognormal / $\mathbb{R}_{\geq 0}$		
$X_7 = \theta_e$ (rad)	$\pi/4$	0.577	uniform / [0, $\pi/2$ ]		
$X_8 = \theta_p \text{ (rad)}$	$\pi/4$	0.577	uniform / [0, $\pi/2$ ]		
$X_9 = \phi_p$ (rad)	π	0.577	uniform / [0,2 $\pi$ [		
$X_{10} = f$ (MHz)	30	0.096	uniform / [25,35]		
$X_{11} = \alpha$ (-)	0.0010	0.289	uniform / [0.0005,0.0015]		

Table 2 – Example 4 - Random inputs.

Limit-state function:

$$g\left(\mathbf{x}\right) = I_{\rm cr} - I\left(\mathbf{x}\right) \, ,$$

where  $I_{\rm cr} = 1.5 \times 10^{-4}$  A is a given current magnitude level to be not exceeded, where

$$I(\mathbf{x}) = \left| \frac{2ha_e}{I_1} I_2 \left[ I_3 \left( I_4 - I_5 \right) + I_6 \right] \right| \quad \text{for } \mathbf{x} = (L, h, d, Z_L, Z_0, a_e, \theta_e, \theta_p, \phi_p, f, \alpha) ,$$

and where:

$$\begin{split} I_{1} &= (Z_{0}Z_{C} + Z_{L}Z_{C})\cosh(\gamma L) + (Z_{C}^{2} + Z_{0}Z_{L})\sinh(\gamma L) ,\\ I_{2} &= \frac{\sin(\beta h\cos\theta_{p})}{\beta h\cos\theta_{p}} ,\\ I_{3} &= i\beta\cos\theta_{p} \left(-\sin\theta_{e}\cos\theta_{p}\sin\phi_{p} + \cos\theta_{e}\cos\phi_{p}\right) ,\\ I_{4} &= \frac{1}{2}(Z_{C} + Z_{0})\frac{\exp\left[\left(\gamma + i\beta\sin\theta_{p}\sin\phi_{p}\right)L\right] - 1}{\gamma + i\beta\sin\theta_{p}\sin\phi_{p}} ,\\ I_{5} &= \frac{1}{2}(Z_{C} - Z_{0})\frac{\exp\left[-\left(\gamma - i\beta\sin\theta_{p}\sin\phi_{p}\right)L\right] - 1}{\gamma - i\beta\sin\theta_{p}\sin\phi_{p}} ,\\ I_{6} &= \sin\theta_{e}\sin\theta_{p} \left[Z_{C} - (Z_{C}\cosh(\gamma L) + Z_{0}\sinh(\gamma L))\exp\left(i\beta L\sin\theta_{p}\sin\phi_{p}\right)\right] , \end{split}$$

in which  $Z_c = 60 \operatorname{acosh}(2h/d)$ ,  $\beta = 2\pi f/3 \times 10^8$  and  $\gamma = \alpha + i\beta$ . In these expressions,  $i = \sqrt{-1}$  is the imaginary number and  $|\cdot|$  denotes the modulus of a complex number.

Reference failure probability:  $p_{\rm fref} = 2.24 \times 10^{-4}$ .

### 5 Example 5

Source: Blatman and Sudret (2010) and Bourinet (2017)



Figure 1 – Example 5. A three-span, five-story, linear elastic frame subjected to lateral loads

Random inputs: A three-span, five-story, linear elastic frame structure subjected to lateral loads is studied in this second example, see Figure 1. The problem has n = 21 random inputs: 3 applied lateral loads, 2 Young's moduli, 8 moments of inertia and 8 cross-sectional areas. This problem was initially proposed by Liu and Der Kiureghian (1986). It was later studied in several research works with differences in the input data. The problem settings here are those of Blatman and Sudret (2010), which specifically considers normal distributions left-truncated at zero for the Young's moduli  $E_{4-5}$ , the moments of inertia  $I_{6-13}$  and the cross-sectional areas  $A_{14-21}$ . The loads  $P_{1-3}$  are assumed independent and lognormally distributed by Blatman and Sudret (2010).

The frame element structural details and the statistical properties of each random input of X are given in Table 3 and 4 respectively. A linear correlation is considered between the following inputs:

- material properties:  $\rho_{E_i E_i} = 0.9$  for  $i, j = 4, 5, i \neq j$ ,
- moments of inertia:  $\rho_{I_i I_i} = 0.13$  for  $i, j = 6, \dots, 13, i \neq j$ ,
- cross-sectional areas:  $\rho_{A_iA_i} = 0.13$  for  $i, j = 14, \dots, 21, i \neq j$ ,
- moment of inertias and cross-sectional areas:  $\rho_{A_i I_j} = \rho_{I_j A_i} = 0.13$  for i = 6, ..., 13, j = 14, ..., 21, except for properties of a single frame element for which we have  $\rho_{A_{i+8}I_i} = \rho_{I_i A_{i+8}} = 0.95$  for i = 6, ..., 13.

Element	Young's modulus	Moment of inertia	Cross-sectional area
$B_1$	$E_4$	<i>I</i> <sub>10</sub>	A <sub>18</sub>
$B_2$	$E_4$	$I_{11}$	A <sub>19</sub>
<i>B</i> <sub>3</sub>	$E_4$	$I_{12}$	A <sub>20</sub>
$B_4$	$E_4$	<i>I</i> <sub>13</sub>	A <sub>21</sub>
$C_1$	<i>E</i> <sub>5</sub>	$I_6$	A <sub>14</sub>
$C_2$	<i>E</i> <sub>5</sub>	I <sub>7</sub>	$A_{15}$
<i>C</i> <sub>3</sub>	<i>E</i> <sub>5</sub>	$I_8$	$A_{16}$
<i>C</i> <sub>4</sub>	<i>E</i> <sub>5</sub>	I <sub>9</sub>	A <sub>17</sub>

Table 3 – Example 5. Frame element properties

X <sub>i</sub>	Mean $\mu_i$	Std dev. $\sigma_i$	$X_i$	Mean $\mu_i$	Std dev. $\sigma_i$	
$P_1$	30	9	$E_4$	454,000	40,000	
$P_2$	20	8	$E_5$	497,000	40,000	
$P_3$	16	6.40				
I <sub>6</sub>	0.94	0.12	A <sub>14</sub>	3.36	0.60	
$I_7$	1.33	0.15	$A_{15}$	4.00	0.80	
$I_8$	2.47	0.30	$A_{16}$	5.44	1.00	
I <sub>9</sub>	3.00	0.35	$A_{17}$	6.00	1.20	
<i>I</i> <sub>10</sub>	1.25	0.30	$A_{18}$	2.72	1.00	
$I_{11}$	1.63	0.40	$A_{19}$	3.13	1.10	
$I_{12}$	2.69	0.65	$A_{20}$	4.01	1.30	

Table 4 – Example 5. Definition of marginal distributions of **X** 

 $\frac{1.09}{3.00} \qquad \begin{array}{c} 1.20 \\ 0.75 \\ \hline A_{21} \\ \hline 4.50 \\ \hline \text{N.B.: } P_i \ , E_i \ , I_i \ , \text{ and } A_i \text{ are respectively in kip, kip/ft}^2, \text{ ft}^4 \text{ and ft}^2.$ 

Limit-state function: Failure is considered when the horizontal displacement  $u_1$  at node 1 exceeds 0.07 cm = 2.2966 × 10<sup>-1</sup> ft, see Figure 1. The LSF reads:

$$g(\mathbf{x}) = g(x_1, \dots, x_{21}) = 0.07 - u_1(\mathbf{x})$$
.

Reference failure probability:  $p_{\rm fref} = 1.05 \times 10^{-4}$ .

 $I_{13}$ 

# 6 Example 6

Source: Bourinet (2018, Chap. 1)

Random inputs:  $U_1, \ldots, U_{16} \sim \mathcal{N}(0, 1), U_1, \ldots, U_{16}$  independent.

Limit-state function:

$$G(\mathbf{u}) = \min_{k \in \{1,...,4\}} G_k(\mathbf{u}) \text{ for } \mathbf{u} = (u_1, ..., u_{16})^{\mathrm{T}},$$

where

$$G_k(\mathbf{u}) = \beta_k - \boldsymbol{\alpha}_k^{\mathrm{T}} \mathbf{u}$$

for  $k = 1, \ldots, 4$ . We take:

$$\beta_1 = 4.0118$$
  $\beta_2 = 4.0109$   $\beta_3 = 4.0108$   $\beta_4 = 4.0051$ ,

and

$\alpha_1 = \langle$	$\left( \begin{array}{c} 0.3040\\ -0.4013\\ 0.2131\\ 0.3218\\ -0.3253\\ 0.2534\\ 0.1582\\ 0.1067\\ 0.2065\\ -0.3173\\ 0.1614\\ 0.2842 \end{array} \right)$	$\langle \alpha_2 = \langle \alpha_$	$\begin{pmatrix} 0.3061 \\ 0.4007 \\ 0.2131 \\ 0.3219 \\ 0.3253 \\ 0.2534 \\ -0.1582 \\ -0.1060 \\ 0.2064 \\ 0.3164 \\ 0.3164 \\ 0.1614 \\ 0.2838 \end{pmatrix}$	$\langle \alpha_3 = \langle \alpha_$	$\begin{pmatrix} 0.3038 \\ 0.4006 \\ -0.2133 \\ 0.3217 \\ -0.3262 \\ -0.2535 \\ -0.1582 \\ 0.1065 \\ 0.2065 \\ 0.3166 \\ -0.1615 \\ 0.2841 \end{pmatrix}$	$\left. \right\} \qquad \boldsymbol{lpha}_4 = \left. \left\{ \right. \right\}$	$ \begin{array}{c} 0.3004 \\ -0.4077 \\ -0.2181 \\ 0.3262 \\ 0.2787 \\ -0.2586 \\ 0.1605 \\ -0.1120 \\ 0.2102 \\ -0.3231 \\ -0.3231 \\ -0.1649 \\ 0.2894 \end{array} $	
-	$\begin{array}{c} -0.3173\\ 0.1614\\ 0.2842\\ -0.2397\\ 0.2022\\ 0.1601\\ 0.1306\end{array}$		$\begin{array}{c} 0.3164\\ 0.1614\\ 0.2838\\ 0.2394\\ 0.2020\\ -0.1600\\ -0.1319\end{array}$		$\begin{array}{r} 0.3166 \\ -0.1615 \\ 0.2841 \\ -0.2396 \\ -0.2023 \\ -0.1603 \\ -0.1319 \end{array}$		$\begin{array}{r} -0.3231 \\ -0.1649 \\ 0.2894 \\ 0.2445 \\ -0.2067 \\ 0.1632 \\ 0.1346 \end{array}$	

Reference failure probability:  $p_{\rm fref} = 1.21 \times 10^{-4}$ .

# 7 Example 7

Source: Dubourg (2011, Chap. 6)

Random inputs:  $U_1, \ldots, U_{93} \sim \mathcal{N}(0, 1), U_1, \ldots, U_{93}$  independent.

Limit-state function:

$$G(\mathbf{u}) = \min_{k \in \{1,...,4\}} G_k(\mathbf{u}) \text{ for } \mathbf{u} = (u_1, ..., u_{93})^{\mathrm{T}},$$

where

$$G_k(\mathbf{u}) = \beta_k - \boldsymbol{\alpha}_k^{\mathrm{T}}\mathbf{u}$$

for k = 1, ..., 4, and

$$\beta_1 = 4.0118$$
  $\beta_2 = 4.0109$   $\beta_3 = 4.0108$   $\beta_4 = 4.0051$ ,

Reference failure probability:  $p_{\rm fref} = 1.22 \times 10^{-4}$ .

## 8 Example 8

Source: Schuëller and Pradlwarter (2007, Problem 3, Case 3.2.1)

Reference failure probability:  $p_{\text{fref}} = 2.41 \times 10^{-4}$ .

# References

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# **Appendix: FERUM-based LSF evaluations**

addpath('/xxx/xxx/FERUM4.1');

#### inputfile\_ex1 % selected input file

```
[probdata,gfundata,analysisopt] = update_data(1,probdata,analysisopt,gfundata,femodel);
probdata.marg = distribution_parameter(probdata.marg);
[ Ro, dRo_drho, dRo_dthetafi, dRo_dthetafj ] = mod_corr_solve(probdata.marg,probdata.correlation,0);
probdata.Ro = Ro;
[ Lo , ierr ] = my_chol(Ro);
probdata.Lo = Lo;
iLo = inv(Lo);
probdata.iLo = iLo;
nrv = size(probdata.marg,1);
nu = 10;
U = randn(nrv,nu); % selected realizations in the standard normal space
X = u_to_x(U,probdata);
```

```
[G, dummy] = gfun(1,X,'no ', probdata, analysisopt, gfundata, femodel, randomfield); % corresponding LSF evaluations
```