

EADS Innovation Works - Applied Mathematics Team

Calibration of a PDE system for thermal regulation of an aircraft cabin

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EADS France - *Applied Mathematics Team*

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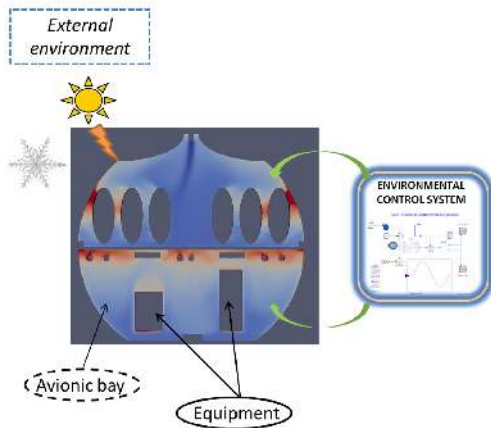
Outline

- 1** Context
- 2** Calibration from experimental data
- 3** Meta model strategy
- 4** Summary & challenges

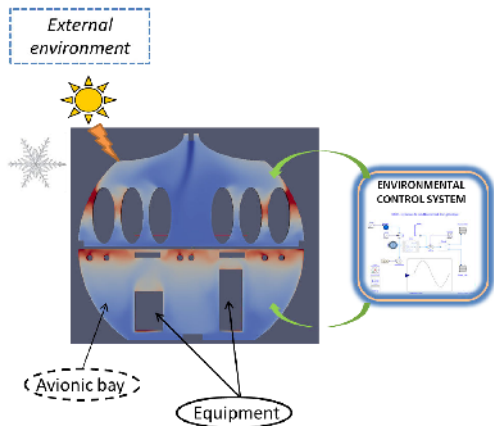
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General context of thermal regulation

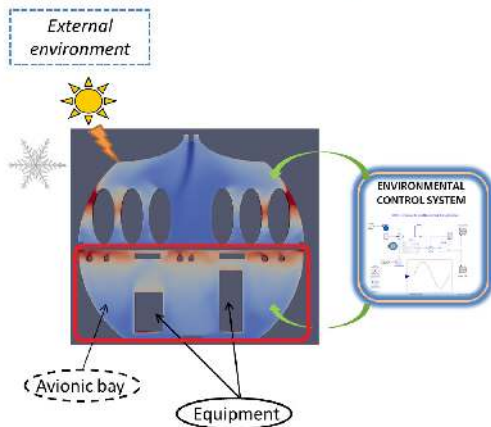


General context of thermal regulation



- Provide thermal comfort & cabin pressurization for crew / passengers
- Thermal control of electric cores or highly dissipative equipment of avionic bay

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Topics of the presentation

Installation of equipment in avionic bay requires the specification of equipment thermal environment

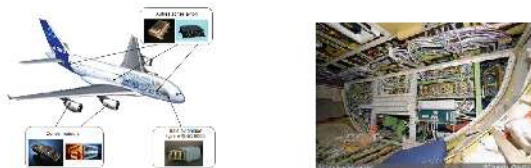
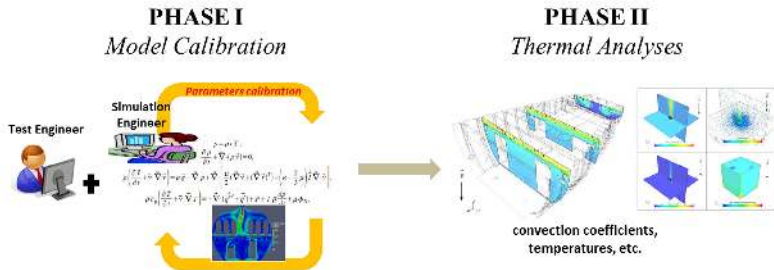


Figure : Aircraft & Equipment - Avionic bay

- Need to provide convection coefficients around the equipment...
- ... For a robust equipment conception

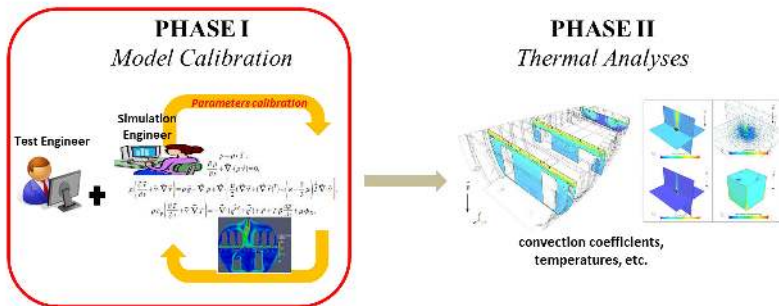
Topics of the presentation



Two phases:

- 1/ PDE parameter estimation
- 2/ Phenomenon study with parametrized PDE

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Modelling

- **(simplified) Thermal exchange modelling** (Navier Stokes equations)

$$\text{Equations : } \left\{ \begin{array}{l} \frac{\partial \rho}{\partial t} + \nabla \cdot (\rho u) = 0 \\ \frac{\partial (\rho C_p T)}{\partial t} + \nabla \cdot (u \cdot \rho C_p T) = \nabla \cdot (k \nabla T) \\ \frac{\partial (\rho u)}{\partial t} + (u \cdot \nabla) u + \nabla p = \mu \Delta u + \rho g \end{array} \right.$$

$$\text{Boundary Conditions : } \left\{ \begin{array}{l} u = u_0(M) \text{ with turbulence model RANS}(\tau) \\ \phi = h_C (T - T_{Skin}) \end{array} \right.$$

ρ = air density, u = air speed, T = temperature, τ = turb. rate, h_C = heat transf. coef., T_{Skin} = skin temp.

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⇒ Lack of knowledge on τ , h_C and T_{Skin} ! ⇐

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- **Input/Output model view**

Equation & Boundary Conditions induce an Input/Output system

$$\mathcal{H}((\tau, T_{Skin}), h_C) .$$

In particular, the post-processing providing convection coefficients is some function $h((\tau, T_{Skin}), h_C)$.

Question ?

How to estimate h_C in presence of uncertainties (τ , T_{Skin}) ?

- We need additional information (reference measures, experimental data, etc.)
- How to model the uncertainties ?
- How to take into account uncertainties in identification procedures ?

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Experiments

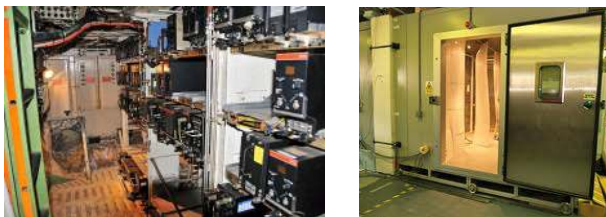


Figure : Flight test - Chamber test

■ Principle:

At a fixed environmental condition, one can measure convection coefficients C_i^{obs} around the equipment.

- Flight tests / Chamber tests
- Few sensors are used

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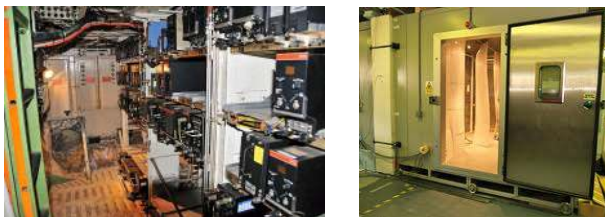


Figure : Flight test - Chamber test

■ **Principle:**

At a fixed environmental condition, one can measure convection coefficients C_i^{obs} around the equipment.

- Flight tests / Chamber tests
- Few sensors are used

Finally, one gets a very precious database (C_i^{obs}) for $i = 1, \dots, N$ with N limited !

Summary

We have two ingredients:

- We can compute convection coefficients of the equipment from Navier Stokes equations

$$C^{comp} = h((\tau, T_{Skin}), h_C)$$

- Experimental database

$$(C_i^{obs})_{i=1, \dots, N}$$

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Q : How to estimate h_C from the experimental database ?

Mathematical formalization

■ Variable of interest (induced by a PDE system)

We call a variable of interest any quantity obtained by a post-processing of some PDE equations resolution. It takes the form

$$h(\mathbf{X}, \theta) \quad \text{field or scalar}$$

where

- $\mathbf{X} \in (\mathbb{R}^d, \mathcal{B}(\mathbb{R}^d), P_{\mathbf{X}})$ is a random vector representing the **uncertainties**
- $\theta \in \mathbb{R}^k$ is the vector of parameters to identify

(in our application: $\mathbf{X} = (\tau, T_{Skin}) \in (\mathbb{R}^2, \mathcal{B}(\mathbb{R}^2), P_{\mathbf{X}})$ and $\theta = h_C \in \mathbb{R}$)

■ Experimental/Reference data (also called Learning data)

It is a set of points:

- $(z_i, Y_i)_{i=1, \dots, N} \rightarrow$ if $h(\mathbf{X}, \theta)$ is a field $z \mapsto h(\mathbf{X}, \theta)[z]$
 - $(Y_l)_{l=1, \dots, N} \rightarrow$ if $h(\mathbf{X}, \theta)$ is scalar
- (Remark: a priori, **There is not** a model linking the observation Y and the simulation $h(\mathbf{X}, \theta)$. For instance, we don't have the regression framework

$$Y = h(\mathbf{X}, \theta) + \varepsilon$$

where ε is the model error. Indeed, **we don't have** joint information $(\mathbf{X}_i, Y_i) !$)

Calibration methods

There are two calibration methods depending on the nature of the variable of interest $h(\mathbf{X}, \theta)$, scalar or field.

Calibration method I (case for fields)

- **Least Squares principle:**

Find parameters $\theta \in \mathbb{R}^k$ which minimize the quantity

$$\mathcal{J}(\mathbf{X}, \theta) = \sum_{i=1}^N (Y_i - h(\mathbf{X}, \theta)[z_i])^2$$

- **Remark !:**

the function $\theta \mapsto \mathcal{J}(\mathbf{X}, \theta)$ to minimize is random (due to uncertainties \mathbf{X}) !

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■ Issue: Stochastic Optimization

Principle: Minimize a quantity $\rho(\mathcal{J}(\mathbf{X}, \theta))$ (deterministic)

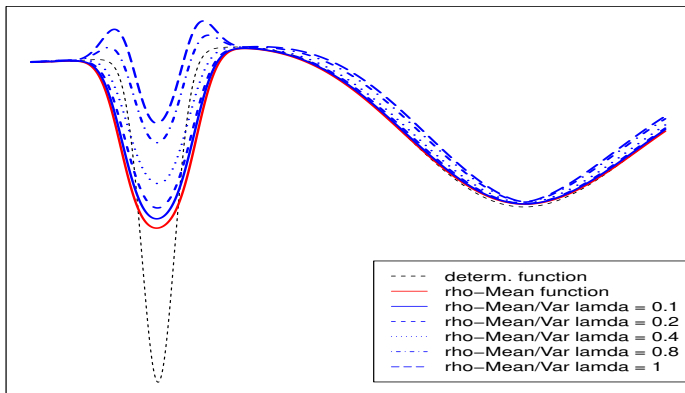
- Mean : $\rho(\mathcal{J}(\mathbf{X}, \theta)) = \mathbb{E}_{\mathbf{X}}(\mathcal{J}(\mathbf{X}, \theta))$
- Variance : $\rho(\mathcal{J}(\mathbf{X}, \theta)) = \text{Var}_{\mathbf{X}}(\mathcal{J}(\mathbf{X}, \theta))$
- Mixed : $\rho_{\lambda}(\mathcal{J}(\mathbf{X}, \theta)) = \mathbb{E}_{\mathbf{X}}(\mathcal{J}(\mathbf{X}, \theta)) + \lambda \sqrt{\text{Var}_{\mathbf{X}}(\mathcal{J}(\mathbf{X}, \theta))}$
- etc.

Calibration method I (case for fields)

■ Illustration

$\theta \mapsto \rho_\lambda(\mathcal{J}(\mathbf{X}, \theta)) = \mathbb{E}_X(\mathcal{J}(\mathbf{X}, \theta)) + \lambda \sqrt{\text{Var}_X(\mathcal{J}(\mathbf{X}, \theta))}$ for different $\lambda > 0$

(deterministic function $\Leftrightarrow \theta \mapsto \mathcal{J}(X_{nom}, \theta)$, where X_{nom} is the nominal value of X)



Calibration method I (case for fields)

- **Stochastic/Robust Optimization**

- **Large literature**



- **Practical algorithms**

Need practical and efficient algorithms ...

Calibration method II (case for scalar outputs)

■ Recall the framework:

- We have observations $(Y_i)_{1, \dots, N}$
- We get a scalar output $h(\mathbf{X}, \theta)$ after a post-processing of a PDE system

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■ Estimation method:

[Rachdi *et al* 2012] Risk bounds for new M-estimation problems, ESAIM:Probability & Statistics, 2012

Principle:

Find parameters $\theta \in \mathbb{R}^k$ which minimize "a distance" between the **empirical distribution** of the Y_i 's and the **simulated distribution** of the random variable $h(\mathbf{X}, \theta)$ (based on a simulated sample $h(\mathbf{X}_1, \theta), \dots, h(\mathbf{X}_m, \theta)$, where $\mathbf{X}_1, \dots, \mathbf{X}_m$ are m simulations of the uncertainty \mathbf{X}).

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- **Example:** Maximum-Likelihood based method

[Rachdi *et al* 2012] Stochastic inverse problem with noisy simulator, Ann. Fac. Sc. Toulouse, 2012

Find θ minimizing

$$\mathcal{J}(\theta) = - \sum_{i=1}^N \log \left(\sum_{j=1}^m K_b(Y_i - h(\mathbf{X}_j, \theta)) \right), \quad \text{with} \quad K_b(y) = \frac{1}{\sqrt{2\pi} b} e^{-y^2/2b^2}$$

Calibration method II (case for scalar outputs)

Theoretical results of the estimator $\hat{\theta}_{N,m}$ where

$$\hat{\theta}_{N,m} = \underset{\theta \in \Theta}{\text{Argmin}} - \sum_{i=1}^N \log \left(\sum_{j=1}^m K_b(Y_i - h(\mathbf{X}_j, \theta)) \right)$$

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Theorem (Consistency) [Rachdi2012]

Denote by f_{θ}^x the density function of $h(\mathbf{X}, \theta)$ and θ^* by

$$\theta^* = \underset{\theta \in \Theta}{\text{Argmin}} - \mathbb{E}(\log(f_{\theta}^x)(Y)) \quad (\text{unknown target}).$$

Under technical conditions, \exists constants c_1, c_2, c_3, a_1 and a_2 such that $\forall 0 < \tau < 1/2$, with probability at least $1 - 2\tau$

$$\|\hat{\theta}_{N,m} - \theta^*\|^2 \leq c_1 \sqrt{\frac{\log(a_1 \tau^{-1})}{N}} + \frac{c_2 \sqrt{\log(a_2 \tau^{-1})} + c_3 m^{1/10}}{\sqrt{m}}.$$

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Theorem (Central Limit Theorem)

In progress !

Simulation of h is limited !

■ Calibration may be very greedy ...

Both calibration methods may need several computations of h involving new PDE system resolutions.

- In most of our applications, one run of h (i.e numerical resolution + post-processing) \sim 6 hours
- So for 50 calibration algorithm iterations, we have to wait \sim 13 days !

■ Strategy adopted:

Replace the CPU time expensive model $h(\mathbf{X}, \theta)$ by a mathematical approximation (analytical) $\tilde{h}(\mathbf{X}, \theta)$, very cheap to evaluate.

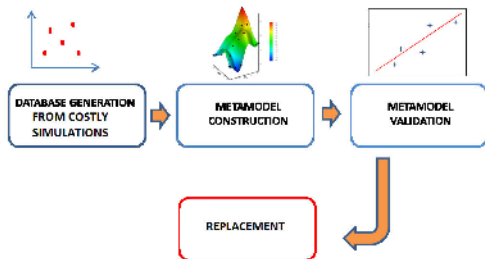
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Meta model strategy

A well adopted strategy (among others...) :

- **Sample, Build, Validate and Replace**



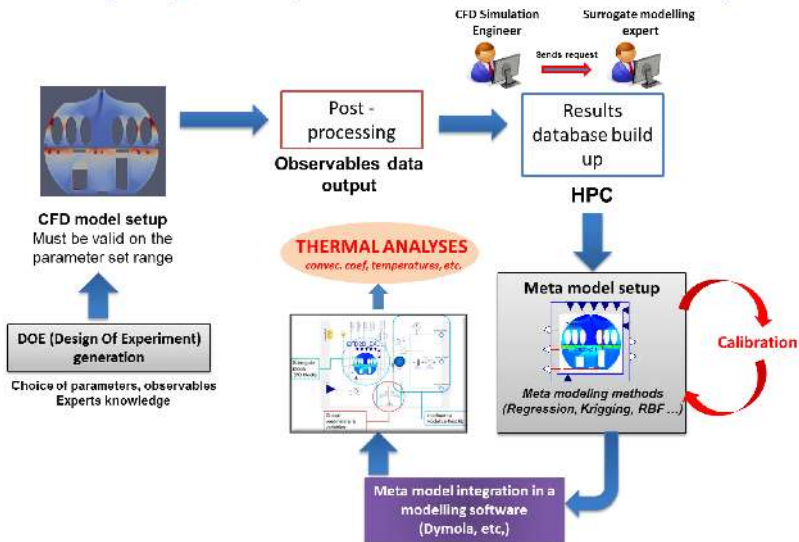
- **Different types of meta models**

- **Regression-based:** (*Neural network, Polynomial Chaos, Least squares, etc.*)
 - **Interpolation-based:** (*Radial Basis Functions, Gaussian processes/Kriging, etc.*)
- Calibration methods only involve the metamodel, i.e one calibrates the metamodel ! (no more the PDE system...)

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Summary : global process of thermal analysis



Conclusions & Issues

- Asymptotic study of the estimator $\hat{\theta}_{N,m}$
- Mathematical study of calibration procedures induced by the Stochastic Optimization of $\theta \mapsto \mathcal{J}(\mathbf{X}, \theta)$
- Quantify the robustness of equipment specification when considering the uncertainties
- Improve existing metamodel-based algorithms (adaptive metamodeling, on-line refinement, etc.)
- HPC capabilities for metamodel constructions
- Facilitate metamodels exportation (distribution to suppliers, etc.)
- Extend the method for Multi-Fidelity learning data (varying mesh size, etc.)

Thank you for your attention !



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