

# Optimization with probabilistic constraints of complex systems

## Application to the design of an offshore wind turbine

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**3** From stationary to piecewise stationary

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## Problem presentation: the stationary case

### ■ Harmonic oscillator (spring/mass system):

- $x_{d_1}$  (mass),  $x_{d_2}$  (spring stiffness),  $x_p$  (damping coefficient);
- Displacement of the object is solution of the oscillator equation:

$$x_{d_1} \mathcal{Y}''(t) + x_p \mathcal{Y}'(t) + x_{d_2} \mathcal{Y}(t) = \eta(t), t \in [0, T].$$

### ■ Introduction of uncertainties:

- uncertainties on  $x_{d_1}, x_{d_2}$  represented by a r.v.  
 $X_d = (X_{d_1}, X_{d_2}), \mathbb{E}[X_d] = d = (d_1, d_2)$  (design variables);
- uncertainties on  $x_p$  represented by a r.v.  $X_p$ ;
- uncertainties on the force:  $\eta(t)$  **stationary Gaussian** random process (with **zero mean** and **known spectral density**).

For fixed  $x_d, x_p$ , the displacement of the object is modelled by the **stochastic process** denoted  $t \rightarrow \mathcal{Y}(x_d, x_p; t)$ .

## Mathematical formulation

### Time-variant Reliability-Based Design Optimization (t-RBDO)

$\min_{d \in \Omega_d} \text{cost}(d)$     such that

$$\mathbb{P}_{X_d, X_p, X_{r_1}, \eta} \left( \max_{t \in [0, T]} \mathcal{Y}'(X_d, X_p; t) > X_{r_1} \right) < p_s$$

$$\mathbb{P}_{X_d, X_p, X_{r_2}, \eta} \left( \max_{t \in [0, T]} \mathcal{Y}''(X_d, X_p; t) > X_{r_2} \right) < p_s$$

$$\mathbb{P}_{X_d, X_p, X_{r_3}, \eta} \left( \int_0^T (|\mathcal{Y}''(X_d, X_p; t)| - \rho)^+ dt > X_{r_3} \right) < p_s$$

with  $(x)^+ = \max\{0, x\}$ . All the sources of uncertainties are **independent**.

#### Difficulty

Estimate the failure probabilities at each iteration of the optimization algorithm. Especially when  $p_s$  is small (rare event).

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## Main reformulation idea

$$\begin{aligned} & \mathbb{P}_{X_d, X_p, X_{r_1}, \eta} \left( \max_{t \in [0, T]} \mathcal{Y}'(X_d, X_p; t) > X_{r_1} \right) \\ &= \mathbb{E}_{X_d, X_p, X_{r_1}} \left[ \mathbb{P}_\eta \left( \max_{t \in [0, T]} \mathcal{Y}'(X_d, X_p; t) > X_{r_1} \right) \right] \end{aligned}$$

Use a limit theorem to approximate  $\mathbb{P}_\eta \left( \max_{t \in [0, T]} \mathcal{Y}'(x_d, x_p; t) > x_{r_1} \right)$  by a quantity that only depends on  $x_d, x_p, x_{r_1}$ .

$$\begin{aligned} & \mathbb{P}_{X_d, X_p, X_{r_2}, \eta} \left( \max_{t \in [0, T]} \mathcal{Y}''(X_d, X_p; t) > X_{r_2} \right) \\ &= \mathbb{E}_{X_d, X_p, X_{r_2}} \left[ \mathbb{P}_\eta \left( \max_{t \in [0, T]} \mathcal{Y}''(X_d, X_p; t) > X_{r_2} \right) \right] \end{aligned}$$

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## Properties of the velocity and acceleration processes

At  $X_d = x_d, X_p = x_p$  fixed:

- $\mathcal{Y}(x_d, x_p; \cdot)$  output of **linear filter**:

$$\mathcal{Y}(x_d, x_p; t) = h_{\mathcal{Y}}(x_d, x_p; \cdot) * \eta(t);$$

- $\eta$  zero-mean Gaussian, stationary with known spectral density.

$\Rightarrow \mathcal{Y}'(x_d, x_p; \cdot)$  and  $\mathcal{Y}''(x_d, x_p; \cdot)$  are also **Gaussian** and **stationary** with **zero mean**. Their spectral moment of order  $n$  is computable from the **spectral density** of  $\eta$ ,  $K_{\eta}$ , and the **transfer function**  $FT(h_{\mathcal{Y}})$ :

$$m_{\mathcal{Y}',n}(x_d, x_p) = \int \omega^{n+2} |FT(h_{\mathcal{Y}})(x_d, x_p; \omega)|^2 K_{\eta}(\omega) d\omega;$$

$$m_{\mathcal{Y}'',n}(x_d, x_p) = \int \omega^{n+4} |FT(h_{\mathcal{Y}})(x_d, x_p; \omega)|^2 K_{\eta}(\omega) d\omega.$$



## Extreme value theory

### Theorem (1)

Let  $\xi$  be zero-mean stationary Gaussian process with spectral moment of order  $n$  denoted  $m_{\xi,n}$ . Then:

$$\mathbb{P} \left( a_T \left( \max_{t \in [0, T]} \frac{\xi(t)}{\sqrt{m_{\xi,0}}} - a_T \right) \leq x \right) \rightarrow \exp(-e^{-x}) \text{ as } T \rightarrow \infty$$

with  $a_T = \sqrt{2 \log \left( \frac{T}{2\pi} \sqrt{\frac{m_{\xi,2}}{m_{\xi,0}}} \right)}$ .

Thus, for  $T$  large enough:

$$\mathbb{P} \left( \max_{[0, T]} \xi(t) \geq x \right) \simeq 1 - \exp \left( -e^{a_T^2 - \frac{a_T x}{\sqrt{m_{\xi,0}}}} \right) = F_\epsilon \left( e^{a_T^2 - \frac{a_T x}{\sqrt{m_{\xi,0}}}} \right)$$

with  $F_\epsilon(x) = 1 - \exp(-x)$ .

[1] Leadbetter et al, *Extremes and Related Properties of Random Sequences and Processes*, Chapter 8, 1983.

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## Reformulation of extreme-based constraints

At fixed  $x_d, x_p$ ,  $\mathcal{Y}'(x_d, x_p; \cdot)$  is a zero-mean stationary Gaussian process.  
 $\Rightarrow$  for  $T$  large enough, we have:

$$\mathbb{P}_\eta \left( \max_{[0, T]} \mathcal{Y}'(x_d, x_p; t) > x_{r_1} \right) \simeq F_\epsilon \left( e^{a_T(x_d, x_p)^2 - \frac{a_T(x_d, x_p)x_{r_1}}{\sqrt{m_{\mathcal{Y}', 0}(x_d, x_p)}}} \right)$$

where  $a_T(x_d, x_p)$  depends on  $T$  and the spectral moments of order 0 and 2 of  $\mathcal{Y}'(x_d, x_p; \cdot)$ . The initial failure probability becomes:

$$\begin{aligned} \mathbb{P}_{X_d, X_p, X_{r_1}, \eta} \left( \max_{t \in [0, T]} \mathcal{Y}'(X_d, X_p; t) > X_{r_1} \right) \\ \simeq \mathbb{E}_{X_d, X_p, X_{r_1}} \left[ F_\epsilon \left( e^{a_T(X_d, X_p)^2 - \frac{a_T(X_d, X_p)X_{r_1}}{\sqrt{m_{\mathcal{Y}', 0}(X_d, X_p)}}} \right) \right] \end{aligned}$$

The same reasoning applies to the second constraint on  $\mathcal{Y}''$ .

## Reformulation of integral-based constraint

For fixed  $x_d, x_p$  fixed,  $(\mathcal{Y}''(x_d, x_p; \cdot) - \rho)^+ = \mathcal{F}(x_d, x_p; \cdot)$  is ergodic:

$$\frac{1}{T} \int_0^T \mathcal{F}(x_d, x_p; t) dt \xrightarrow{\mathbb{P}} \mathbb{E}_{\mathcal{F}}[\mathcal{F}(x_d, x_p; 0)] \quad \text{as } T \rightarrow \infty.$$

Hence, for T large enough:

$$\mathbb{P}_{\eta} \left( \int_0^T \mathcal{F}(x_d, x_p; t) dt > x_{r_3} \right) \simeq \mathbb{1}_{T\mathbb{E}_{\mathcal{F}}[\mathcal{F}(x_d, x_p; 0)] > x_{r_3}}.$$

We only need  $m_{\mathcal{Y}''_0}(x_d, x_p)$  to compute  $\mathbb{E}_{\mathcal{F}}[\mathcal{F}(x_d, x_p; 0)]$ . The failure probability becomes:

$$\begin{aligned} \mathbb{P}_{X_d, X_p, X_{r_3}, \eta} \left( \int_0^T \mathcal{F}(X_d, X_p; t) dt > X_{r_3} \right) \\ \simeq \mathbb{E}_{X_d, X_p} [F_{r_3}(T\mathbb{E}_{\mathcal{F}}[\mathcal{F}(X_d, X_p; 0)])] \end{aligned}$$

with  $F_{r_3}$  the cumulative distribution function of  $X_{r_3}$ .

## Reformulated problem

### Reliability-Based Design Optimization (RBDO)

$\min_{d \in \Omega_d} \text{cost}(d)$     such that

$$\mathbb{E}_{X_d, X_p, X_{r1}} \left[ F_\epsilon \left( e^{a_T(X_d, X_p)^2 - \frac{a_T(X_d, X_p)X_{r1}}{\sigma_{y'}(X_d, X_p)}} \right) \right] < p_s$$

$$\mathbb{E}_{X_d, X_p, X_{r2}} \left[ F_\epsilon \left( e^{b_T(X_d, X_p)^2 - \frac{b_T(X_d, X_p)X_{r2}}{\sigma_{y'}(X_d, X_p)}} \right) \right] < p_s$$

$$\mathbb{E}_{X_d, X_p} \left[ F_{r3} \left( T \mathbb{E}_{\mathcal{F}} [\mathcal{F}(X_d, X_p; 0)] \right) \right] < p_s$$

#### Remark

Time-independent RBDO: easier to solve.

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## Definition of a piece-wise stationary process

- The period  $[0, T]$  is decomposed into  $n_T$  intervals  
 $I_i = [(i-1)\Delta T, i\Delta T], i = 1, \dots, n_T$ .
- for fixed  $x_d, x_p$  the process  $\mathcal{Y}(x_d, x_p; \cdot)$  is defined as:

$$\mathcal{Y}(x_d, x_p; t) = \sum_{i=1}^{n_T} \mathcal{Y}_i(x_d, x_p, S_i; t) \mathbb{1}_{I_i}(t)$$

where  $\mathcal{Y}_i(x_d, x_p, S_i; t)$  is solution of the oscillator equation with external force  $\eta(S_i, t)$ .

- $S_1, \dots, S_{n_T}$  are i.i.d. discrete random variables such that  $\mathbb{P}(S_1 = s^j) = p^j$  for  $j = 1, \dots, 7$ .
- $\eta(s^j, \cdot)$  is a zero-mean stationary Gaussian process with spectral density depending on  $s^j$ .

## Reformulated problem

### Reliability-Based Design Optimization (RBDO)

$\min_{d \in \Omega_d} \text{cost}(d)$  such that

$$\mathbb{E}_{X_d, X_p, X_{r_1}} \left[ F_\epsilon \left( \sum_{j=1}^7 e^{a_{Tpj} (X_d, X_p, s^j)^2 - \frac{a_{Tpj} (X_d, X_p, s^j) X_{r_1}}{\sqrt{m_{y',0}(X_d, X_p, s^j)}}} \right) \right] < p_s$$

$$\mathbb{E}_{X_d, X_p, X_{r_2}} \left[ F_\epsilon \left( \sum_{j=1}^7 e^{b_{Tpj} (X_d, X_p, s^j)^2 - \frac{b_{Tpj} (X_d, X_p, s^j) X_{r_2}}{\sqrt{m_{y'',0}(X_d, X_p, s^j)}}} \right) \right] < p_s$$

$$\mathbb{E}_{X_d, X_p} \left[ F_{r_3} \left( T \sum_{j=1}^7 p^j \mathbb{E}_{\mathcal{F}_1} [\mathcal{F}_1 (X_d, X_p, s^j; 0)] \right) \right] < p_s$$



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## Metamodeling strategy

First constraint:

$$\begin{aligned} p_1(d) &= \mathbb{E}_{X_d, X_p, X_{r_1}} \left[ F_\epsilon \left( \sum_{j=1}^7 e^{a_{T_p j} (X_d, X_p, s^j)^2 - \frac{a_{T_p j} (X_d, X_p, s^j) X_{r_1}}{\sqrt{m_{y', 0}(X_d, X_p, s^j)}}} \right) \right] \\ &= \mathbb{E}_{X_d, X_p, X_{r_1}} \left[ F_\epsilon \left( \sum_{j=1}^7 e^{M(X_d, X_p, X_{r_1}, s^j)} \right) \right] \end{aligned}$$

From a space-filling design of experiments (DoE) of the **augmented space**, calibration of a metamodel by **Kriging**:

$$\tilde{M}(x_d, x_p, x_{r_1}, s^j) \sim \mathcal{N}(\mu(x_d, x_p, x_{r_1}, s^j), \sigma(x_d, x_p, x_{r_1}, s^j)^2)$$

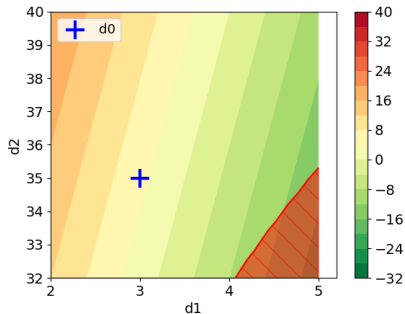
- Idea of AK-ECO : succession of cycles composed of a local enrichment of the metamodels and an optimization resolution.

## Solving the RBDO problem: AK-ECO

**Initialization:** Initial design  $d^0$ , DoE  $DoE^0$  and metamodel  $\tilde{M}^0$ , cycle  $k = 1$ .

**Optimization cycle  $k$ :**  $d^{k-1}$ ,  $\tilde{M}^{k-1}$ ,  $DoE^{k-1}$

- **Step 1:** local enrichment of the metamodel:
  - Step 1.a: accuracy criterion
  - Step 1.b: selection of  $x_{enr}$ . Update  $DoE^{k-1}$  and recalibration of  $\tilde{M}^{k-1}$ .
- $DoE^{k-1} \rightarrow DoE^k$  and  $\tilde{M}^{k-1} \rightarrow \tilde{M}^k$ .
- **Step 2:** solve the reformulated RBDO starting from  $d^{k-1}$ .
  - optimization algorithm chosen by user + constraints evaluated with Monte Carlo replacing  $M$  by  $\tilde{M}^k \rightarrow d^k$ .
- **Stopping condition:**
  - If  $\|d^k - d^{k-1}\| < \epsilon$  OR  $|cost(d^k) - cost(d^{k-1})| < \epsilon$ : AK-ECO ends and  $d^{min} = d^k$ .
  - Else:  $k = k + 1$  and go back to step 1.

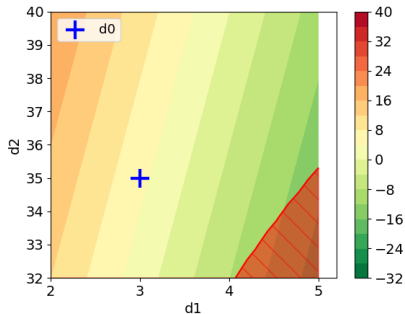


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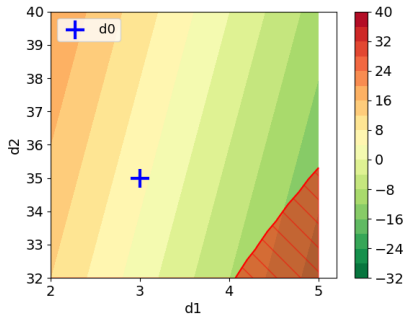
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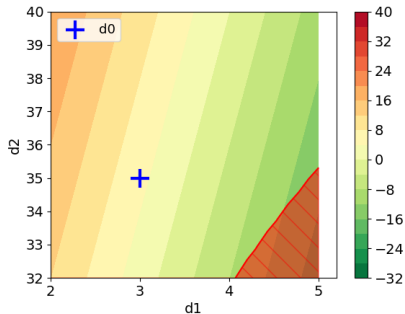
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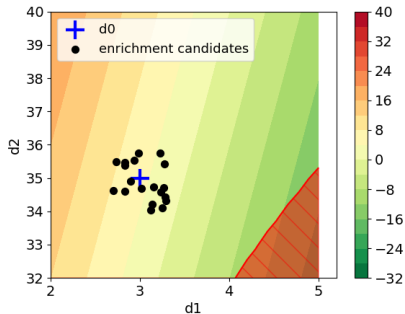
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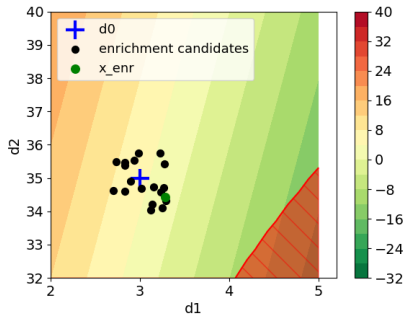
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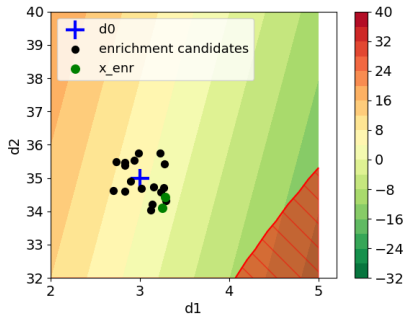
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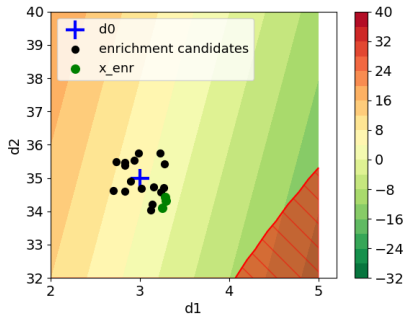
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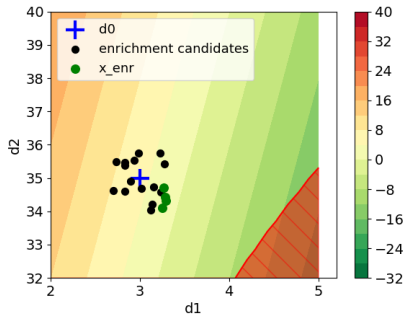
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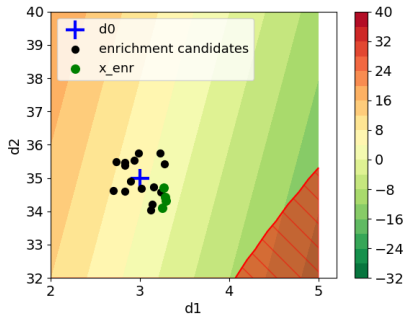
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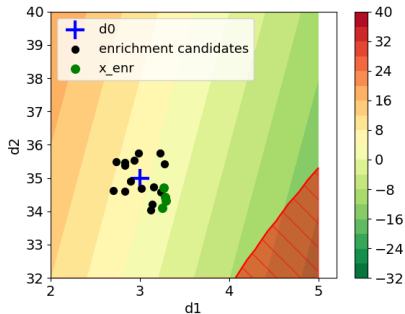


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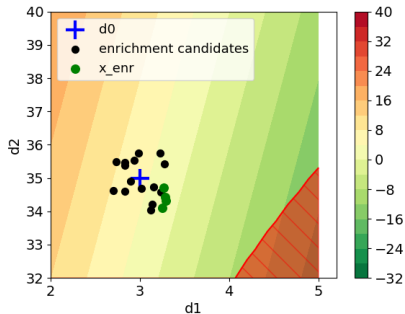


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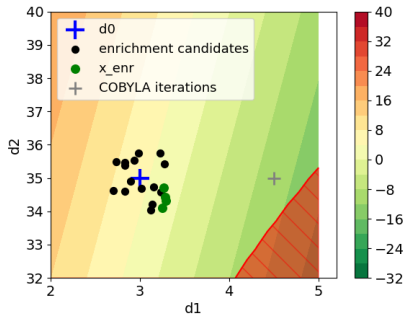


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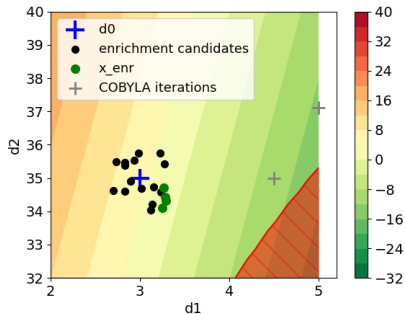
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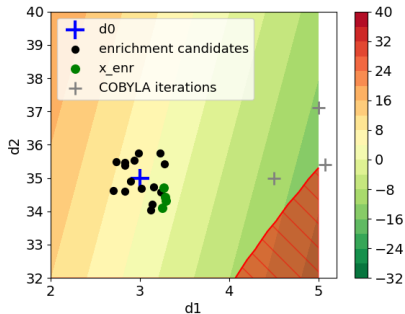


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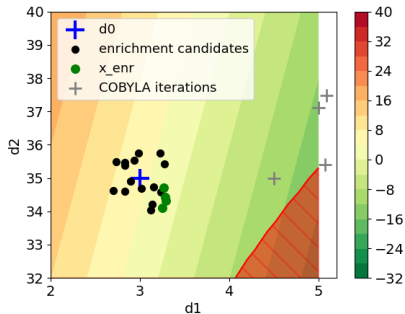
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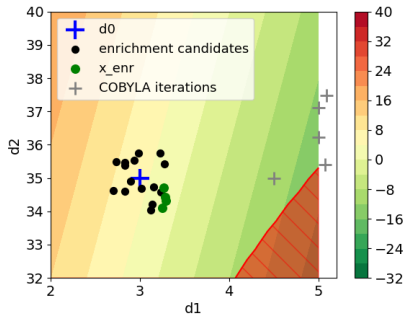
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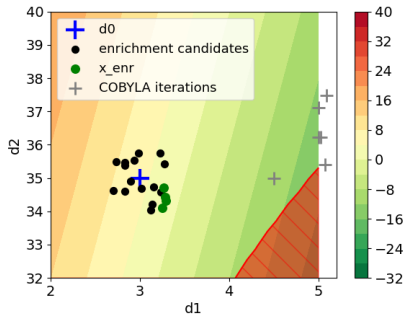
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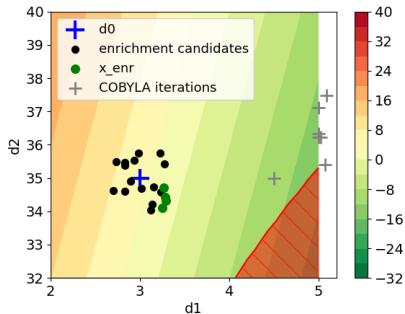
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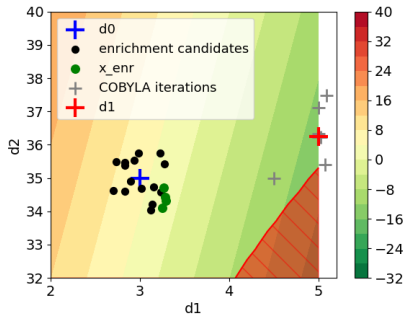
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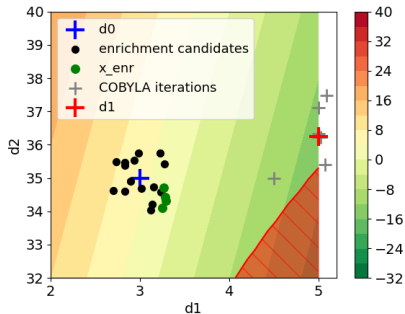
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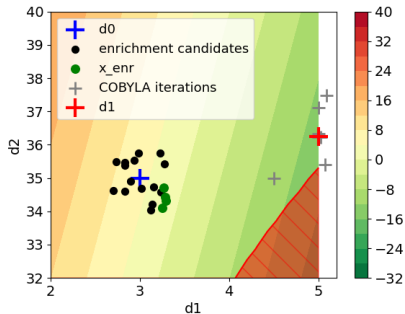
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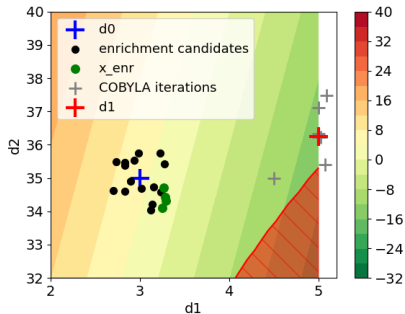


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## Comparison of AK-ECO with reference methods in RBDO

Results of different methods starting from  $d^0 = (3, 35)$ :

	MC	RIA[2]	PMA[2]	SORA[3]	Stieng[4]	AK-ECO
$d^{min}$	(5.0, 35.78)	(5.0, 35.07)	(5.0, 35.04)	(5.0, 36.06)	(4.98, 37.82)	(5.0, 35.67)
$cost(d^{min})$	-14.22	-14.93	-14.96	-13.94	-11.89	-14.33
$p_1^{MC} \left( d^{min} \right)$	$0.6 \times 10^{-4}$	$0.7 \times 10^{-4}$	$0.8 \times 10^{-4}$	$0.5 \times 10^{-4}$	$0.1 \times 10^{-4}$	$0.5 \times 10^{-4}$
$p_2^{MC} \left( d^{min} \right)$	$1.0 \times 10^{-4}$	$1.0 \times 10^{-4}$	$1.4 \times 10^{-4}$	$0.7 \times 10^{-4}$	$0.3 \times 10^{-4}$	$1.0 \times 10^{-4}$
$p_3^{MC} \left( d^{min} \right)$	$0.1 \times 10^{-4}$	$0.4 \times 10^{-4}$	$0.4 \times 10^{-4}$	$0.1 \times 10^{-4}$	$0.02 \times 10^{-4}$	$0.2 \times 10^{-4}$
$n_{call}$	$3.36 \times 10^6$	431256	29393	16072	32242	150

**Table:** Results of AK-ECO and the comparison methods

- ▶ AK-ECO finds a reliable optimum with few calls to the expensive code.

[2] J. Tu, K.K. Choi and Y. H. Park. *A New Study on Reliability-Based Design Optimization*, Journal of Mechanical Design, 1999.

[3] X. Du and W. Chen, *Sequential Optimization and Reliability Assessment Method for Efficient Probabilistic Design*, Journal of Mechanical Design, 2004

[4] Lars Einar S. Stieng. *Optimal design of offshore wind turbine support structures under uncertainty*. PhD thesis, Norwegian University of Science and Technology, 2019.

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**Table:** Results of AK-ECO and the comparison methods

- ▶ AK-ECO finds a reliable optimum with few calls to the expensive code.

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[3] X. Du and W. Chen, *Sequential Optimization and Reliability Assessment Method for Efficient Probabilistic Design*, Journal of Mechanical Design, 2004

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- 1 Presentation of the harmonic oscillator problem
- 2 Problem reformulation
- 3 From stationary to piecewise stationary
- 4 Solving the reformulated problem with AK-ECO
- 5 Conclusion**





## Conclusion

- **Optimization problem with probabilistic constraints** dependent on **random variables** and a **piecewise-stationary stochastic Gaussian process**: t-RBDO.
- Methodology in two parts:
  - Reformulation of the constraints using **limit theorems**;
  - Resolution of the reformulated problem with a **new adaptive kriging strategy AK-ECO**.
- Application of the methodology to the harmonic oscillator problem.
- Not presented work:
  - Quantification of the approximation errors made during the reformulation steps;
  - Global enrichment of the metamodels before AK-ECO;
  - RBDO-oriented GSA;
  - Application of the methodology to the FOWT problem [5].

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[5] A.Cousin, J. Garnier, M. Guiton, M. Munoz Zuniga. *Optimization with probabilistic constraints of complex systems. Application to the design of an offshore wind turbine*. ECCOMAS, 2021

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# 6 Appendix

## General formulation

$\min_{d \in \Omega_d} \text{cost}(d)$     such that

$$\mathbb{P}_{X_d, X_p, X_{r_I}, \mathcal{Y}} \left( \min_{[0, T]} \mathcal{Y}(X_d, X_p; t) > X_{r_I} \right) < p_s$$

$$\mathbb{P}_{X_d, X_p, X_{r_{II}}, \mathcal{Y}} \left( \int_0^T f(\mathcal{Y}(X_d, X_p; t)) dt > X_{r_{II}} \right) < p_s.$$



## Graphs of the PW stationary oscillator problem

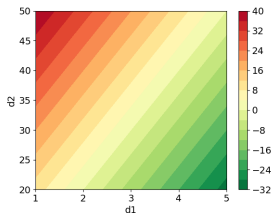


Figure: Level sets of the cost function

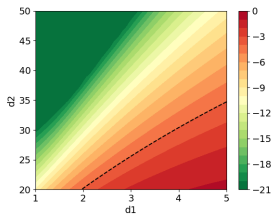


Figure: Level sets of the log of  $p_1$

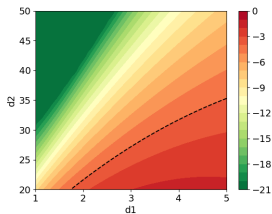


Figure: Level sets of the log of  $p_2$

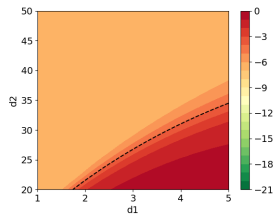


Figure: Level sets of the log of  $p_3$

## Reformulated constraints: probability version

Reformulated failure probabilities as expectations:

$$\mathbb{E}_{X_d, X_p, X_{r_I}} \left[ F_\epsilon \left( \sum_{j=1}^{n_s} e^{M_I(X_d, X_p, X_{r_I}, s^j)} \right) \right] < p_s \quad (1)$$

$$\mathbb{E}_{X_d, X_p} \left[ F_{r_{II}} \left( \sum_{j=1}^{n_s} T p^j (M_{II}(X_d, X_p, s^j)) \right) \right] < p_s \quad (2)$$

with  $F_\epsilon(x) = 1 - \exp(-x)$ .

Reformulated failure probabilities as probabilities:

$$\mathbb{P}_{X_d, X_p, X_{r_I}, X_\epsilon} \left( X_\epsilon - \sum_{j=1}^{n_s} \exp(M_I(X_d, X_p, X_{r_I}, s^j)) < 0 \right) < p_s, \quad (3)$$

$$\mathbb{P}_{X_d, X_p, X_{r_{II}}} \left( X_{r_{II}} - \sum_{j=1}^{n_s} T p^j (M_{II}(X_d, X_p, s^j)) < 0 \right) < p_s \quad (4)$$

with  $X_\epsilon$  r.v with exponential distribution of parameter 1.

## AK-ECO Step 1.a: accuracy criterion

$$p_1^{k-1}(d^{k-1}) = \frac{1}{N_{MC}} \sum_{i=1}^{N_{MC}} F_\epsilon \left( \sum_{j=1}^7 \exp \left( \mu^{k-1} \left( x_{d^{k-1}}^i, x_p^i, x_{r_1}^i, s^j \right) \right) \right) \quad (5)$$

$$p_{I,-}^{k-1}(d) = \frac{1}{n_{MC}} \sum_{i=1}^{n_{MC}} F_\epsilon \left( \sum_{j=1}^{n_s} \exp \left( \mu_I^{k-1} \left( x_d^i, x_p^i, x_{r_1}^i, s^j \right) \right) - 2\sigma_I^{k-1} \left( x_d^i, x_p^i, x_{r_1}^i, s^j \right) \right) \quad (6)$$

$$p_{I,+}^{k-1}(d) = \frac{1}{n_{MC}} \sum_{i=1}^{n_{MC}} F_\epsilon \left( \sum_{j=1}^{n_s} \exp \left( \mu_I^{k-1} \left( x_d^i, x_p^i, x_{r_1}^i, s^j \right) \right) + 2\sigma_I^{k-1} \left( x_d^i, x_p^i, x_{r_1}^i, s^j \right) \right) \quad (7)$$

Accuracy criteria for the first constraint:

$$\frac{|p_1^{k-1}(d^{k-1}) - p_s|}{p_{I,+}^{k-1}(d^{k-1}) - p_{I,-}^{k-1}(d^{k-1})} > 1.$$

## AK-ECO Step 1.b: enrichment criterion

$$p_1^{k-1} (d^{k-1}) = \frac{1}{N_{MC}} \sum_{i=1}^{N_{MC}} F_\epsilon \left( \sum_{j=1}^7 e^{\mu^{k-1}(x_{d^{k-1}}^i, x_p^i, x_{r_1}^i, s^j)} \right)$$

$$\max_{i \in \{1, \dots, N_{MC}\}, j \in \{1, \dots, 7\}} \mathcal{C}_{aug}(x_{d^{k-1}}^i, x_p^i, x_{r_1}^i, s^j) \quad \text{with} \quad \mathcal{C}_{aug}(x_d^i, x_p^i, x_{r_1}^i, s^j)$$

$$= \left[ F_\epsilon \left( \sum_{j' \neq j} e^{\mu^{k-1}(x_d^i, x_p^i, x_{r_1}^i, s^{j'})} + e^{(\mu^{k-1}(x_d^i, x_p^i, x_{r_1}^i, s^j) + 2\sigma^{k-1}(x_d^i, x_p^i, x_{r_1}^i, s^j))} \right) \right. \\ \left. - F_\epsilon \left( \sum_{j' \neq j} e^{\mu^{k-1}(x_d^i, x_p^i, x_{r_1}^i, s^{j'})} + e^{(\mu^{k-1}(x_d^i, x_p^i, x_{r_1}^i, s^j) - 2\sigma^{k-1}(x_d^i, x_p^i, x_{r_1}^i, s^j))} \right) \right] \\ \times f_{X_d, X_p, X_{r_1}}(x_d^i, x_p^i, x_{r_1}^i)$$

$F_\epsilon(x) = 1 - \exp(-x)$  and  $f_{X_d, X_p, X_{r_1}}$  the pdf of  $(X_d, X_p, X_{r_1})$