



DE LA RECHERCHE À L'INDUSTRIE

Inverse uncertainty quantification of input model parameters in thermal-hydraulic simulation

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Context and motivations

- ▶ Needed to simulate power plants (innovative or in operation) as well as for safety analyses of hypothetical accidental scenarios.
- ▶ Simulations run by **Best Estimate** computer codes with a great effort to V&V (ex: the CATHARE code in CEA).
- ▶ Based on balance equations (mass, momentum and energy) which require **closure models** due to time and space averaging.
- ▶ Example: the energy equation applied to a control volume:

$$\rho \overbrace{\frac{\partial I}{\partial t}}^{(1)} = - \overbrace{\text{grad}(\dot{q}'')}^{(2)} + \overbrace{\dot{q}'''}^{(3)} + \overbrace{\frac{\partial P}{\partial t}}^{(4)} + \overbrace{\phi}^{(5)}$$

(1) variation in time of enthalpy, **(2) and (3) are heat fluxes which should be modeled by (semi)-empirical models**, (4) variation in time of the pressure, (5) dissipation function.

"Nominal" closure models:

- ▶ Established by means of both expertise and well-chosen experimental data, and denoted by

$$M_{nom}(\mathbf{x}),$$

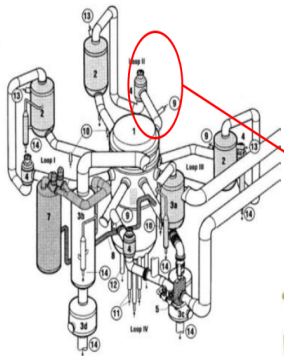
with \mathbf{x} being thermal-hydraulic and design variables,

- ▶ Experimental uncertainty on \mathbf{x} may occur but is often neglected in practice.

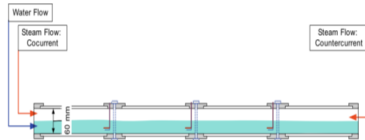
Simulations:

- Implemented from appropriate closure models \implies numerical uncertainties to check (verification task).
- Comparisons between the simulations and corresponding experimental data (validation task).
- Assessment of model uncertainty from the discrepancy between the two \implies **IUQ (inverse uncertainty quantification)**.

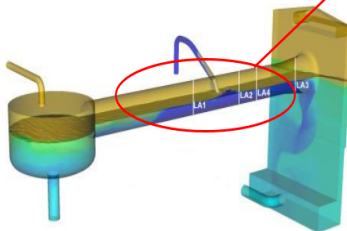
Integral Effect Tests (IETs)



Separated Effect Tests (SETs)



Combined Effect Tests (CETs)



The CIRCE method

CIRCE = *Calcul des Incertitudes Relatives aux Corrélations Élémentaires* (De Crécy and Bazin, 2001).

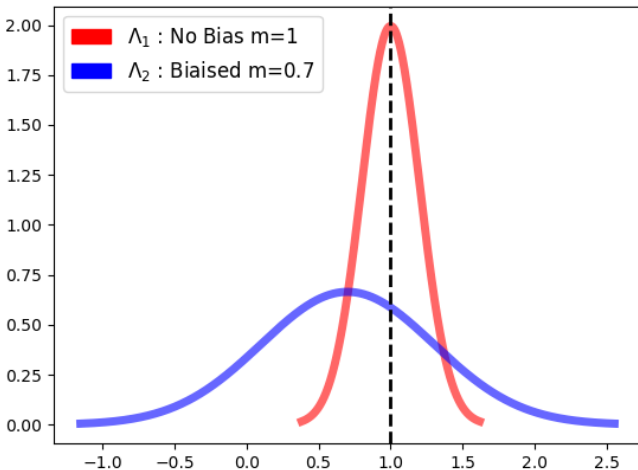
Main assumptions:

- Model uncertainty is multiplicative:

$$M_\lambda(\mathbf{x}) = \lambda \times M_{nom}(\mathbf{x})$$

- λ is modeled as a probability distribution $\implies M_\lambda$ is aleatory,
- λ is Gaussian $\mathcal{N}(m, \sigma^2)$,
- Model uncertainty is known as "unbiased" if $m = 1$.

We wish that the bias, equal to $1 - \hat{m}$, is as small as possible.



Probabilistic link between the experimental data and simulations:

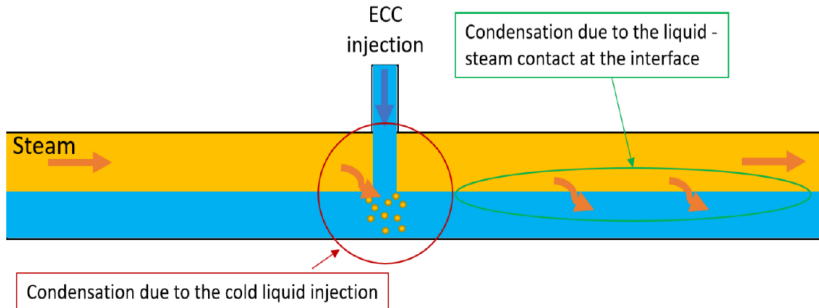
- $y_i \in \mathbb{R}$ the experimental QoI at \mathbf{x}_i (for $i \in \llbracket 1; n \rrbracket$),
- G the CATHARE code (used as a black-box),
- We assume that

$$\begin{aligned}
 y_i &= G(\overbrace{M_{\lambda_{1,i}}(\mathbf{x}_i), \dots, M_{\lambda_{p,i}}(\mathbf{x}_i)}^{\text{Aleatory closure models}}) + \epsilon_i \\
 &= G_{\lambda_i}(\mathbf{x}_i) + \epsilon_i
 \end{aligned}$$

where

- $\lambda_i = (\lambda_{1,i}, \dots, \lambda_{p,i})^T \in \mathbb{R}^p$ with $\lambda_{j,i} \sim \mathcal{N}(m_j, \sigma_j^2)$, $j \in \llbracket 1; p \rrbracket$.
- $\epsilon_i \sim \mathcal{N}(0, \sigma_{\epsilon_i}^2)$.

The CIRCE method jointly estimates all the m_j and σ_j^2
(SETs: $p = 1$, CETs: $p \geq 2$).



This is a CET: $p = 2$ condensation phenomena, modeled respectively by $M_{\lambda_1}(\cdot)$ and $M_{\lambda_2}(\cdot)$, take place at the same time.

CIRCE consists of three main steps:

- 1) Linearization of the simulations in λ at the nominal model, i.e. $\lambda^* = \mathbf{1}_p$

$$y_i - G_{\lambda^*}(\mathbf{x}_i) = h_i^T (\lambda_i - \lambda^*) + \epsilon_i, \quad i \in \llbracket 1; n \rrbracket.$$

- 2) Joint computation of **Maximum Likelihood estimates** $(\hat{m}_j, \hat{\sigma}_j^2)$ if $H = [h_1, \dots, h_n]^T \in \mathcal{M}_{n,p}(\mathbb{R})$ is full rank.
- 3) Confirmation of the results through a posterior inspection of both linearity and normality assumptions.

In this presentation, we are focusing on the second step!

- ▶ Mean parameters $m := (m_1, \dots, m_p)^T \in \mathbb{R}^p$,
- ▶ Variance parameters $\sigma^2 := (\sigma_1^2, \dots, \sigma_p^2)^T \in \mathbb{R}^p$,
- ▶ Shifted observed data $Y := (y_1 - G_{\lambda^*}(\mathbf{x}_1), \dots, y_n - G_{\lambda^*}(\mathbf{x}_n))^T \in \mathbb{R}^n$,
- ▶ Shifted latent data $\lambda := (\lambda_1 - \lambda^*, \dots, \lambda_n - \lambda^*)^T \in \mathcal{M}_{n,p}(\mathbb{R})$,
- ▶ Shifted complete data $Z := \{Y, \lambda\}$.

- **Complete likelihood:** $L(Z|m, \sigma^2) = \overbrace{L(Y|\lambda, m, \sigma^2)}^{\text{Gaussian}} \overbrace{L(\lambda|m, \sigma^2)}^{\text{Gaussian}}$ with

$$L(Y|\lambda, m, \sigma^2) \propto \prod_{i=1}^n \exp\left(-\frac{1}{2} \frac{(Y_i - h_i^T \lambda_i)^2}{\sigma_{\epsilon_i}^2}\right)$$

and

$$L(\lambda|m, \sigma^2) \propto \prod_{i=1}^n |\text{diag}(\sigma^2)|^{-1/2} \exp\left(-\frac{1}{2} (\lambda_i - m)^T \text{diag}(\sigma^2)^{-1} (\lambda_i - m)\right).$$

- **Marginal likelihood:** integrating over λ leads to the likelihood of the observed data only, still Gaussian:

$$L(Y|m, \sigma^2) \propto \prod_{i=1}^n (h_i^T \text{diag}(\sigma^2) h_i + \sigma_{\epsilon_i}^2)^{-1/2} \exp\left(-\frac{1}{2} \frac{(Y_i - h_i^T m)^2}{h_i^T \text{diag}(\sigma^2) h_i + \sigma_{\epsilon_i}^2}\right).$$

ECME = *Expectation-Conditional Maximization Either* (Celeux et al., 2010)

1. Step of Expectation (E): calculation of

$$Q((m, \sigma^2), (m^k, \sigma^{2,k})) = \mathbb{E}_\lambda[l(Z|m, \sigma^2)|Y, m^k, \sigma^{2,k}].$$

The expectation is taken with respect to the distribution of λ conditional on $(Y, m^k, \sigma^{2,k})$.

2. Steps of Conditional Maximization (CM):

- CM1: $\sigma^{2,k+1} = \operatorname{argmax} Q((m, \sigma^2), (m^k, \sigma^{2,k}))$,
- CM2: $m^{k+1} = \operatorname{argmax}_m^{\sigma^2} l(Y|m^k, \sigma^{2,k+1})$.

- ▶ CM1 and CM2 have **analytic expressions** as functions of $(m^k, \sigma^{2,k})$.
- ▶ Starting from a first sample (m_0, σ_0^2) , the convergence of the ECME algorithm is **faster than that of EM**.

CIRCE on CETs

- ▶ $p \geq 2$ factors estimated jointly from Y , often in a small data context ($50 \leq n \leq 200$),
- ▶ If $H_{*1} \gg H_{*2}$ (case $p = 2$), then the estimators $(\hat{m}_2, \hat{\sigma}_2^2)$ and $(\hat{m}_1, \hat{\sigma}_1^2)$ may be respectively inaccurate and degraded.

Multi-stage CIRCE: (Cocci et al., 2022)

- ▶ CETs can still be used, but to estimate only the dominant factor, say λ_1 , while neglecting the other ones,
- ▶ If being known, the uncertainty of the other factors λ_j ($2 \leq j \leq p$) adds up to the experimental uncertainty (case $p = 2$ below):

$$Y_i = h_{i1}\lambda_{1,i} + \epsilon_i \quad \text{with} \quad \epsilon_i \sim \mathcal{N}(h_{i2}m_2, h_{i2}^2\sigma_2^2 + \sigma_{\epsilon_i}^2).$$

$$\iff$$

$$Y_i - h_{i2}m_2 = h_{i1}\lambda_{1,i} + \epsilon_i \quad \text{with} \quad \epsilon_i \sim \mathcal{N}(0, h_{i2}^2\sigma_2^2 + \sigma_{\epsilon_i}^2).$$

Multi-group CIRCE

Motivation:

The model uncertainty may not be the same across the whole set of experimental tests Y . How to statistically check on it?

- ▶ Y is now made up of s groups of different experimental setups:

$$Y := (Y_1, \dots, Y_s, \dots, Y_l)^T \in \mathbb{R}^n \quad ; \quad 1 \leq s \leq l$$

- ▶ A variance parameter σ_s^2 is estimated for each group jointly to a mean parameter m common to every group.
- ▶ For example, Y_s may have a specific geometry or thermal-hydraulic input range.
- ▶ Let i_s denote the last index of the s -th group. Then,

$$i_{s-1} + 1 \leq i \leq i_s \quad \implies \quad \lambda_i \sim \mathcal{N}(m, \sigma_s^2)$$

Multi-group complete likelihood:

$$L(Z|m, \sigma_1^2, \dots, \sigma_l^2) = L(Y|\lambda, m, \sigma_1^2, \dots, \sigma_l^2) L(\lambda|m, \sigma_1^2, \dots, \sigma_l^2)$$

with

$$L(\lambda|m, \sigma_1^2, \dots, \sigma_l^2) \propto \prod_{s=1}^l \prod_{i=i_{s-1}+1}^{i_s} \left[|\text{diag}(\sigma_s^2)|^{-1/2} \exp \left(-\frac{1}{2} (\lambda_i - m)^T \text{diag}(\sigma_s^2)^{-1} (\lambda_i - m) \right) \right].$$

Both E. and CM. steps of the multi-group ECME are **still analytic**, and thus the MLE is readily computable.

We aim to evaluate the degree of statistical evidence that the variances of the groups are different to one another.

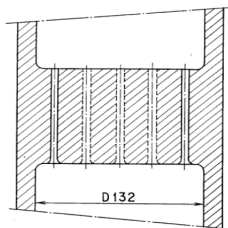
- ▶ Null hypothesis: $\mathcal{H}_0 : \sigma_s^2 - \sigma_{s'}^2 = 0, \quad 1 \leq s \neq s' \leq l.$
- ▶ The **Wald's statistic** is written as:

$$W = \frac{(\hat{\sigma}_s^2 - \hat{\sigma}_{s'}^2)^2}{\mathbb{V}[\hat{\sigma}_s^2] + \mathbb{V}[\hat{\sigma}_{s'}^2] - 2\text{Cov}(\hat{\sigma}_s^2, \hat{\sigma}_{s'}^2)} \sim \chi^2(1) \text{ under } \mathcal{H}_0,$$

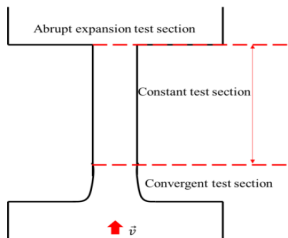
with $\chi^2(1)$ denoting the chi-square distribution with one degree of freedom.

- ▶ The test can be applied to each pair of indexes $1 \leq s \neq s' \leq l.$

- ▶ Discharge of coolant flow due to pressure drop at the break.
- ▶ The mass flow rate reaches a maximum value called **critical mass flow** (or choked flow).
- ▶ Several types of SETs for this phenomenon, including BETHSY Nozzle 2 (B2) and BETHSY Nozzle 6 (B6).



a) BETHSY 2"



b) BETHSY 6"

Is the uncertainty influenced by the geometry?

- ▶ $p = 1$: M_{nom} is the so-called flashing model,
- ▶ $Y = Y_{B2} \cup Y_{B6}$ with $n_{B2} = 25$ and $n_{B6} = 24$,
- ▶ Simulations run with the CATHARE code,
- ▶ Log-Linearization was more accurate $\implies \lambda \sim \mathcal{LN}(m, \sigma^2)$,
- ▶ The multi-group ECME gives:

$$\hat{m} = 0.57 \quad \text{and} \quad (\hat{\sigma}_{B2}^2, \hat{\sigma}_{B6}^2) = (0.31, 0.13).$$

- ▶ $W = 3.62$ and $\mathbb{P}[\chi^2(1) \leq 3.84] = 0.95$. The equality of variances is thus not rejected at the 5% level.

Related works

- ▶ Non-linear CIRCE ([Barbillon et al., 2011](#)), Bayesian CIRCE ([Damblin and Gaillard, 2020](#)).
- ▶ Assessment of the **adequacy** of experimental databases through the criteria of representativeness and completeness ([Baccou et al., 2019](#)).
- ▶ On going-OCDE project, named **ATRIUM**, on the realization of IUQ methods by numerous worldwide participants.
- ▶ **Scaling issue**: do the uncertainties remain valid on IETs or ultimately on an actual power plant?

- Baccou, J., Zhang, J., Fillion, P., Damblin, G., Petruzzi, A., Mendizábal, R., Reventós, F., Skorek, T., Couplet, M., looss, B., Oh, D.-Y., and Takeda, T. (2019). Development of good practice guidance for quantification of thermal-hydraulic code model input uncertainty. *Nuclear Engineering and Design*, 354 :110173.
- Barbillon, P., Celeux, G., Grimaud, A., Lefebvre, Y., and De Rocquigny, E. (2011). Nonlinear methods for inverse statistical problems. *Computational Statistics and Data Analysis*, 55(1) :132–142.
- Celeux, G., Grimaud, A., Lefebvre, Y., and de Rocquigny, E. (2010). Identifying intrinsic variability in multivariate systems through linearized inverse methods. *Inverse Problems in Science and Engineering*, 18.
- Cocci, R. (2022). *Statistical Learning and inverse uncertainty quantification in nuclear thermal-hydraulic simulation : application to the condensation modelling at the safety injection*. PhD thesis, Université Paris Saclay.
- Cocci, R., Damblin, G., Ghione, A., Sargentini, L., and Lucor, D. (2022). Extension of the circe methodology to improve the inverse uncertainty quantification of several combined thermal-hydraulic models. *Nuclear Engineering and Design*, 398.
- Damblin, G., Bachoc, F., Gazzo, S., Sargentini, L., and Ghione, A. (2023). A generalization of the circe method for quantifying input model uncertainty in presence of several groups of experiments. *Submitted to Nuclear Engineering and Design*.
- Damblin, G. and Gaillard, P. (2020). Bayesian inference and non-linear extensions of the circe method for quantifying the uncertainty of closure relationships integrated into thermal-hydraulic codes. *Nuclear Engineering and Design*, 369(6).
- De Crécy, A. and Bazin, P. (2001). Determination of the uncertainties of the constitutive relationship of the CATHARE 2 code. *M&C Salt Lake City, Utah, USA*.