



An approach to evaluate uncertainties in complex CFD simulations

Romain CAMY
romain.camy@edf.fr

Research Engineer
EDF R&D

November 2013

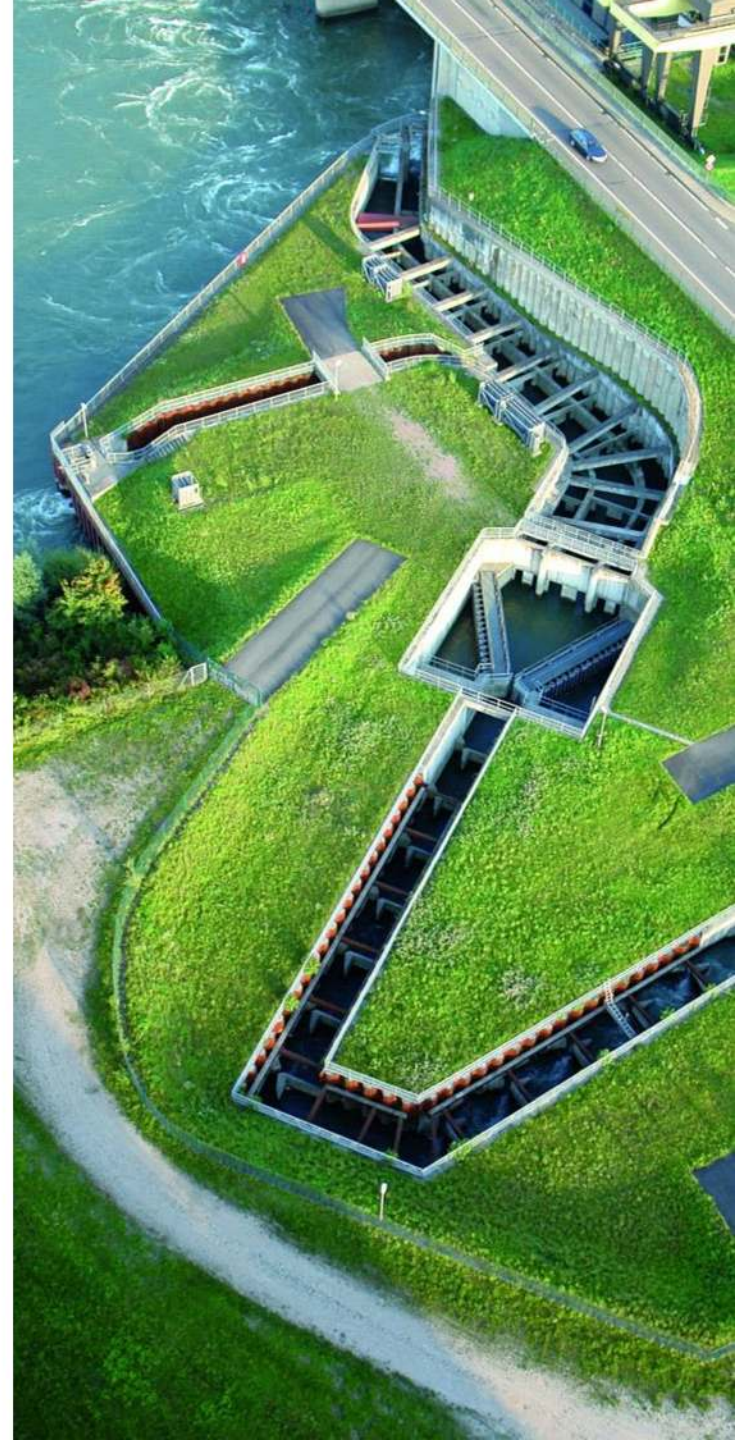


Table of content

1. A practical example
2. A chaotic industrial flow example
3. A pragmatic approach (ICARE)
4. Step-by-step description of the procedure
5. Results in an actual R&D nuclear study
6. Conclusions and short term prospects

A practical example

- We consider a simple physical phenomenon: the crushing load y of a given mechanical part made of a given material as a function of its thickness x .

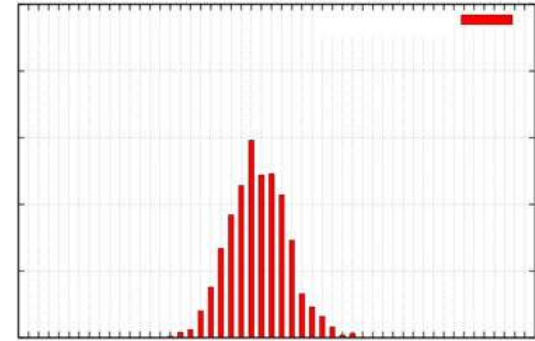
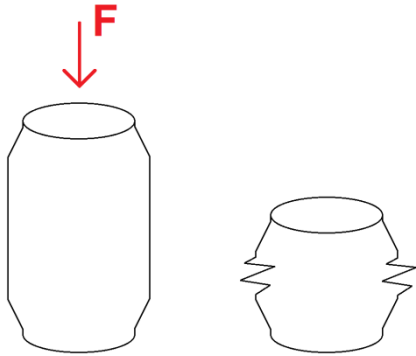
$$y = f(x)$$

- What is expected (implicitly most of the time):

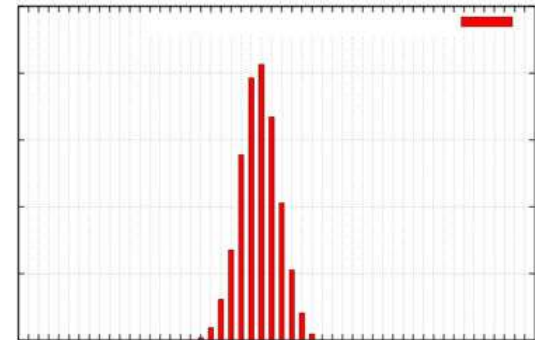
$$\lim_{\varepsilon \rightarrow 0} f(x + \varepsilon) = f(x)$$

A practical example

- If we do the experiment with for example soda cans. We measure wall thickness and record the load $y=F$ when it crushes \rightarrow big dispersion for small variations of thickness.



- Further, if we select cans with the same thickness (according to our measurements) we will still get a significant dispersion.



A practical example

- What happened here is that at our macroscopic scale, identical cans exhibit different crushing load. It seems that:

$$\lim_{\varepsilon \rightarrow 0} f(x + \varepsilon) \neq f(x)$$

- Reasons are:
 - Cans are actually not identical
 - Physical equations are strongly non linear
- Consequences if you had to calculate how many cans can be stacked one over the other for transportation: you would have uncertainty on that number even if at your macroscopic scale, there is no uncertainty on cans material, thickness and so on.
- Unfortunately, fluid mechanics equations are also strongly non linear.
- Fortunately, uncertainties propagation takes necessarily this extra uncertainty source into account.

A chaotic industrial flow example

- Objective: Assess thermal load uncertainties in a Pressurized Thermal Shock (PTS) transient following a Loss Of Coolant Accident (LOCA).
- At EDF R&D Chatou, we develop an open source Computational Fluid Dynamics (CFD) code. *Code_Saturne* (<http://code-saturne.org>).



- Numerical PWR PTS transient (simulation with *Code_Saturne*):
 - [REP ICARE x5.avi](#)

A chaotic industrial flow example

- At EDF R&D Chatou, we also operate a 0.5 scale mock-up of a Pressurized Water Reactor (PWR) primary loop (experimental setup about 5m high):



- Experimental HYBISCUS II test case:
 - [HII ICARE exp.avi](#)
- Numerical HYBISCUS II test case (simulation with *Code_Saturne*):
 - [HII ICARE.avi](#)

A pragmatic approach (ICARE)

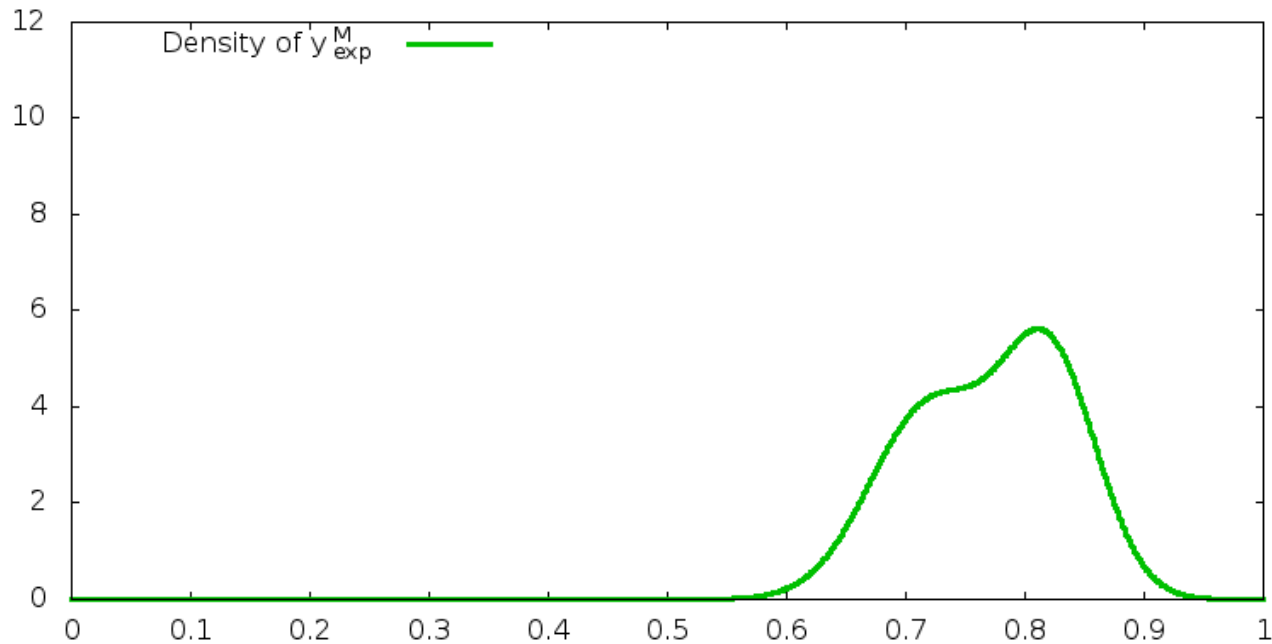
- 9 Sources of uncertainties identified
 1. Approximate physical models
 2. Discretisation error
 3. Convergence error
 4. Round-off errors
 5. Error in geometry definition
 6. Domain limitation error
 7. Oversight of influencing physical phenomena
 8. Uncertain input physical parameters
 9. Error arising from chaotic behaviour

- Dealing with all of them is intractable in complex simulations → rely on experimental data from integral validation¹ experimental test cases to estimate 7 first points.

¹ integral validation experimental test case : Means a test case that is for a certain physics fully representative of the considered full scale device.

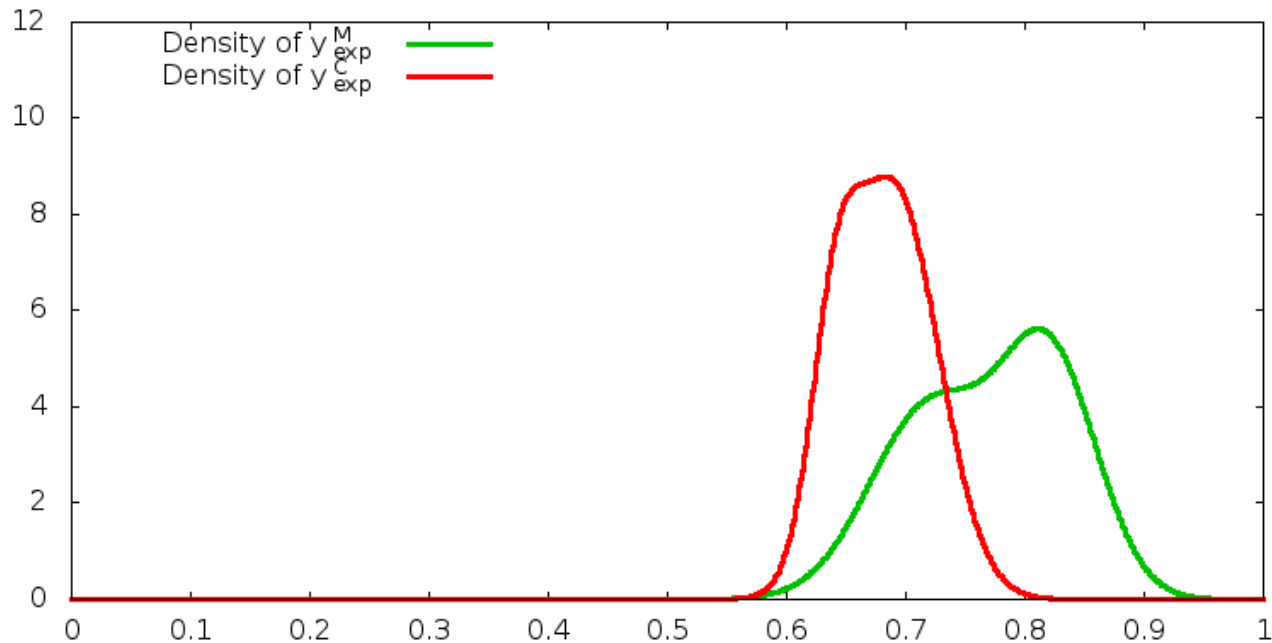
Step-by-step description of the procedure

- We consider an integral validation experiment repeated n_{exp} times.
- We consider the n_{exp} measures of these n_{exp} experiments (here and after, measure is supposed to be reality). If the experiments have chaotic features, one will get significant dispersion for very similar conditions $\underline{x}_{\text{exp},i}^M$, $i \in [1, n_{\text{exp}}]$.



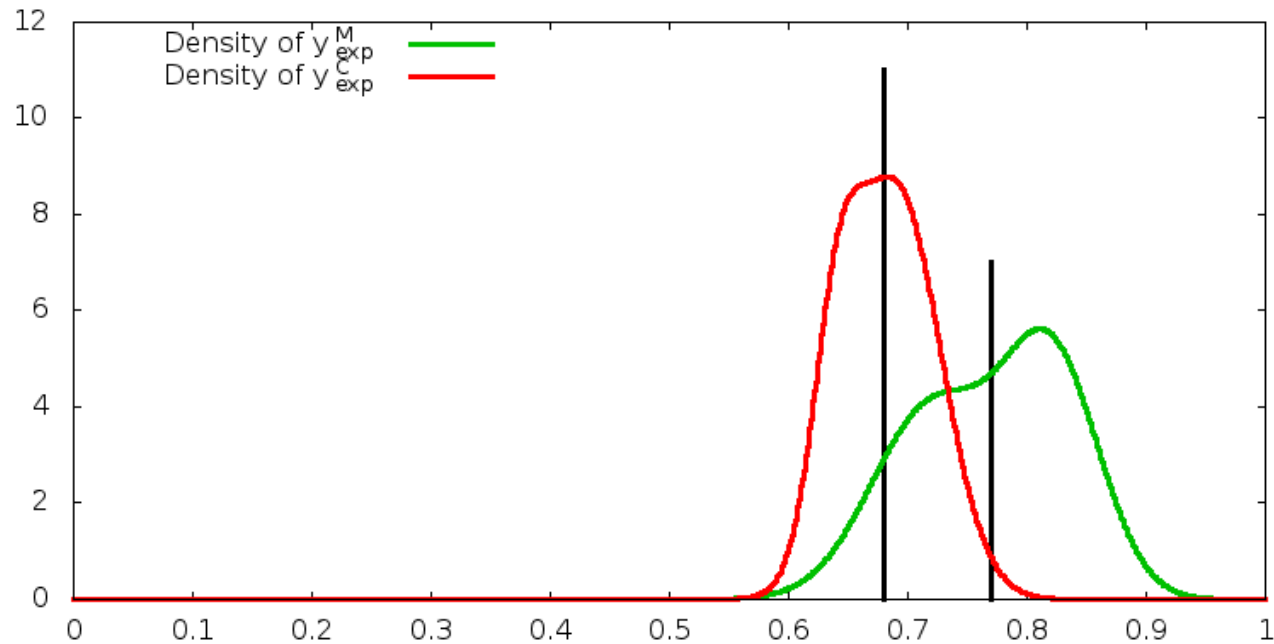
Step-by-step description of the procedure

- We make n_{exp} calculations with our Model and the n_{exp} sets of measured experimental conditions $\underline{x}_{\text{exp},i}^M$. Each calculation corresponds to a particular experimental run.
- If physics is chaotic, the calculations have to reproduce this behavior and lead to a dispersion comparable to the one of measures.



Step-by-step description of the procedure

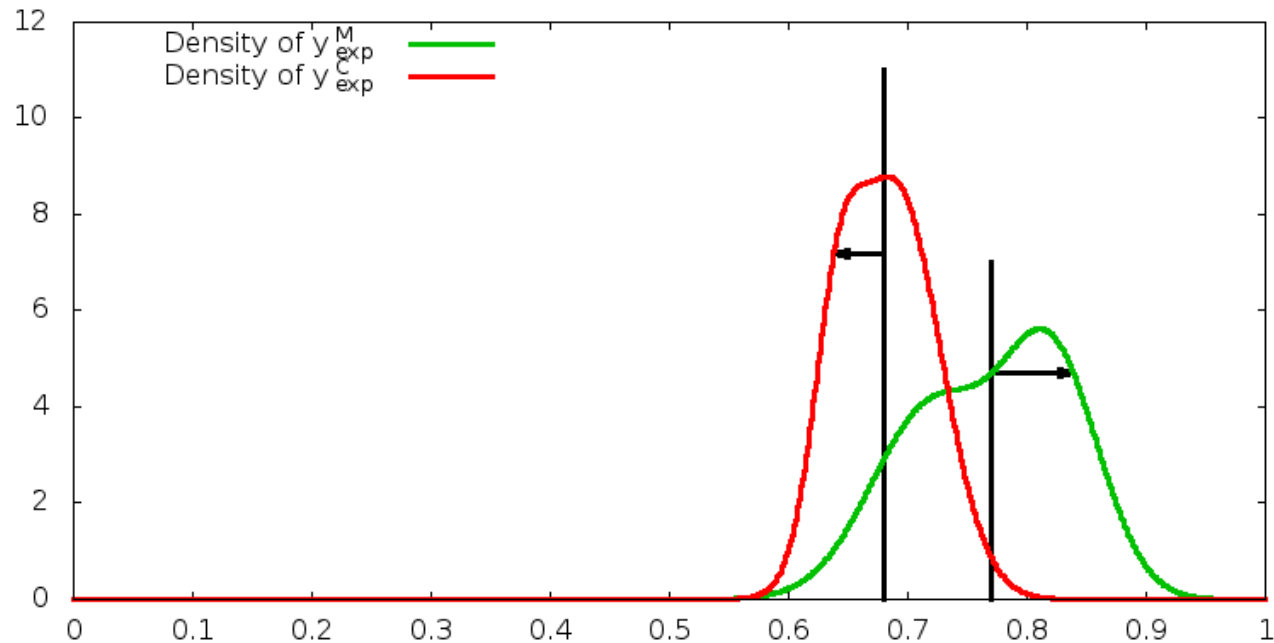
- We calculate mean values for both measured and calculated results.



Step-by-step description of the procedure

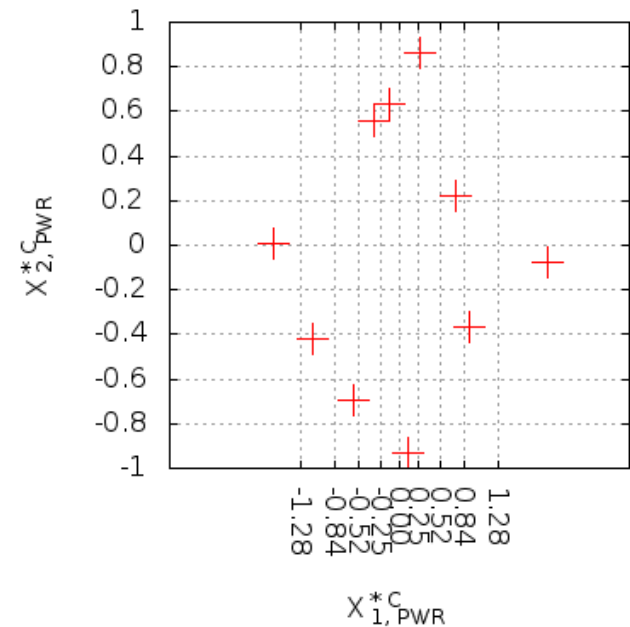
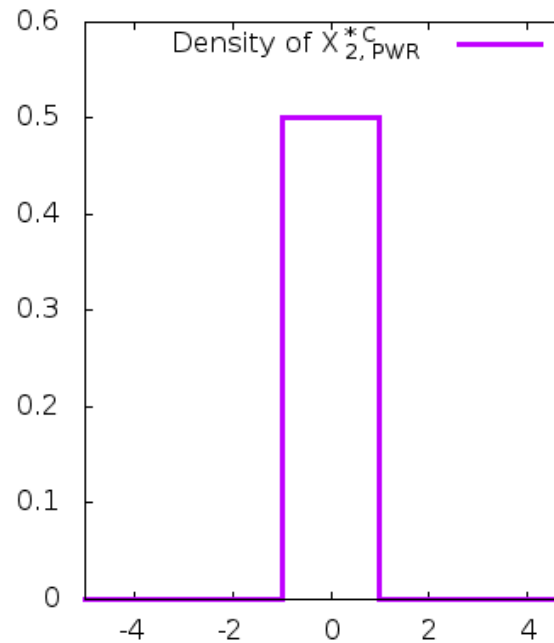
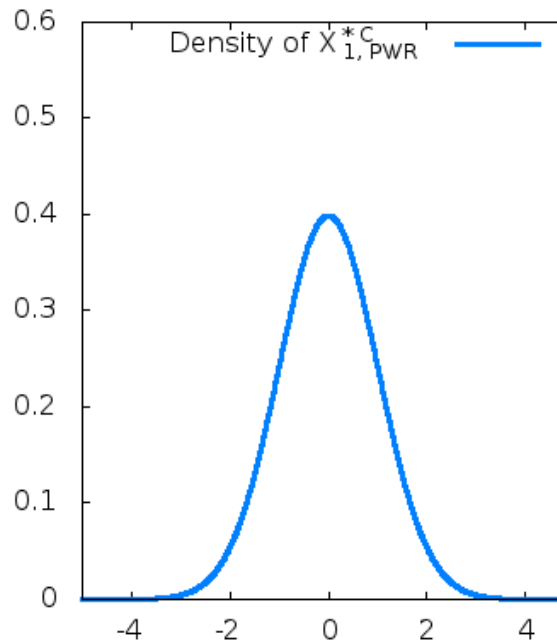
- We calculate standard deviations for both measured and calculated results.
- We quantify Model error by considering ratios of mean values and standard deviations:

$$\frac{\mu_{\text{exp}}^{\text{M}}}{\mu_{\text{exp}}^{\text{C}}}, \frac{\sigma_{\text{exp}}^{\text{M}}}{\sigma_{\text{exp}}^{\text{C}}}$$



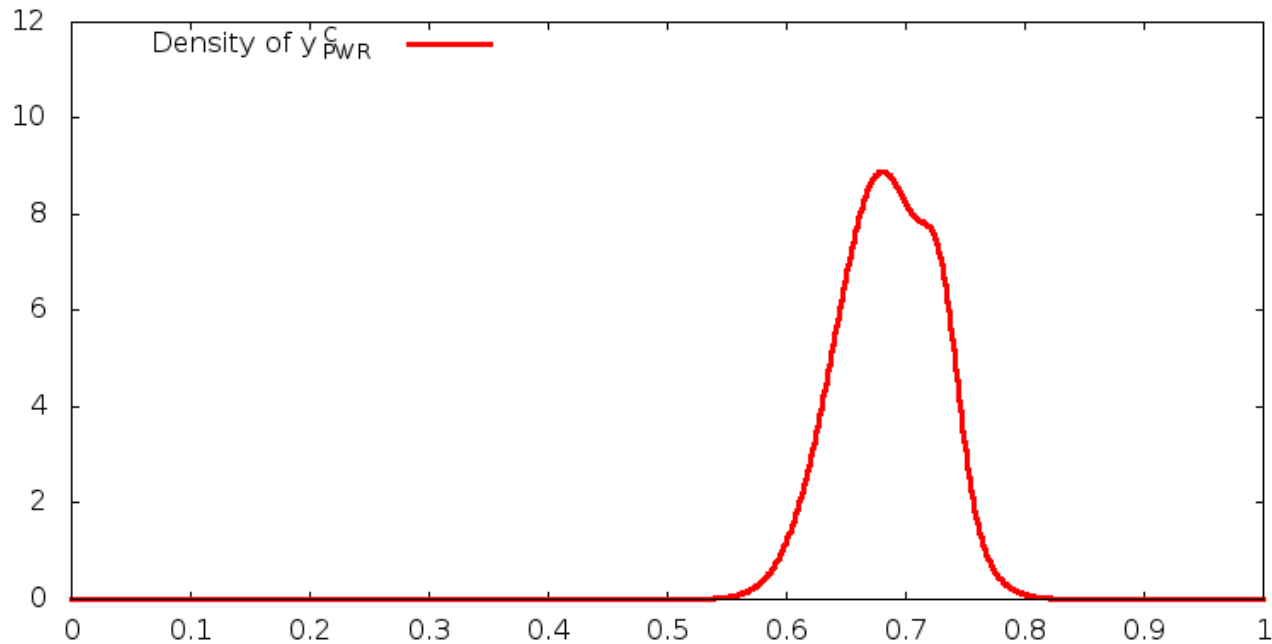
Step-by-step description of the procedure

- We consider our Model at industrial scale case. The industrial and test case Models have to be similar (similar characteristic length, similar non dimensional numbers and similar non dimensional results).
- We consider uncertain input parameters of the Model used at industrial scale and create a Design Of Experiments (DOE) of n_{PWR} points accordingly.



Step-by-step description of the procedure

- Propagation of uncertainties gives n_{PWR} calculation results (we have no measures at industrial scale) having a dispersion due to:
 - significant variations in the input ;
 - inherent variability of the physics.

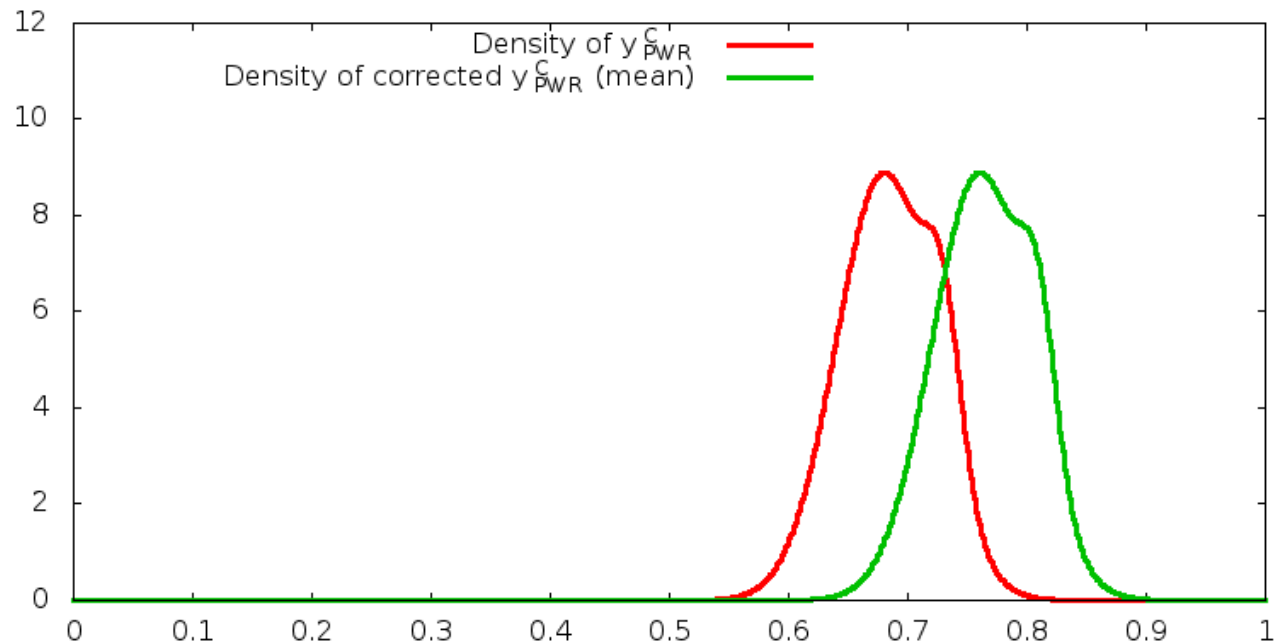


Step-by-step description of the procedure

- We can correct each calculation result with the tendency, observed at test case scale, to under- / over- estimate average value:

$$\varphi(y_{PWR}^C) = y_{PWR}^C \frac{\mu_{exp}^M}{\mu_{exp}^C}$$

- Geometrically, it results in a translation of the density.



Step-by-step description of the procedure

- To correct each calculation result with the tendency, observed at test case scale, to under- / over- estimate inherent variability of the results we need to isolate at industrial scale inherent variability from variability due to significant variations of input parameters.
- This separation requires an estimation of the expectancy of $y_{\text{PWR}}^{\text{C}}$ conditional to $\underline{x}_{\text{PWR}}^{\text{C}}$. It can be done with a regression and a least square estimation of the coefficients, for example:

$$\mu_{\text{PWR}}^{\text{C}}(\underline{x}_{\text{PWR}}^{\text{C}}) = \sum_{j=1}^{n_x} a_j x_j + a_0$$

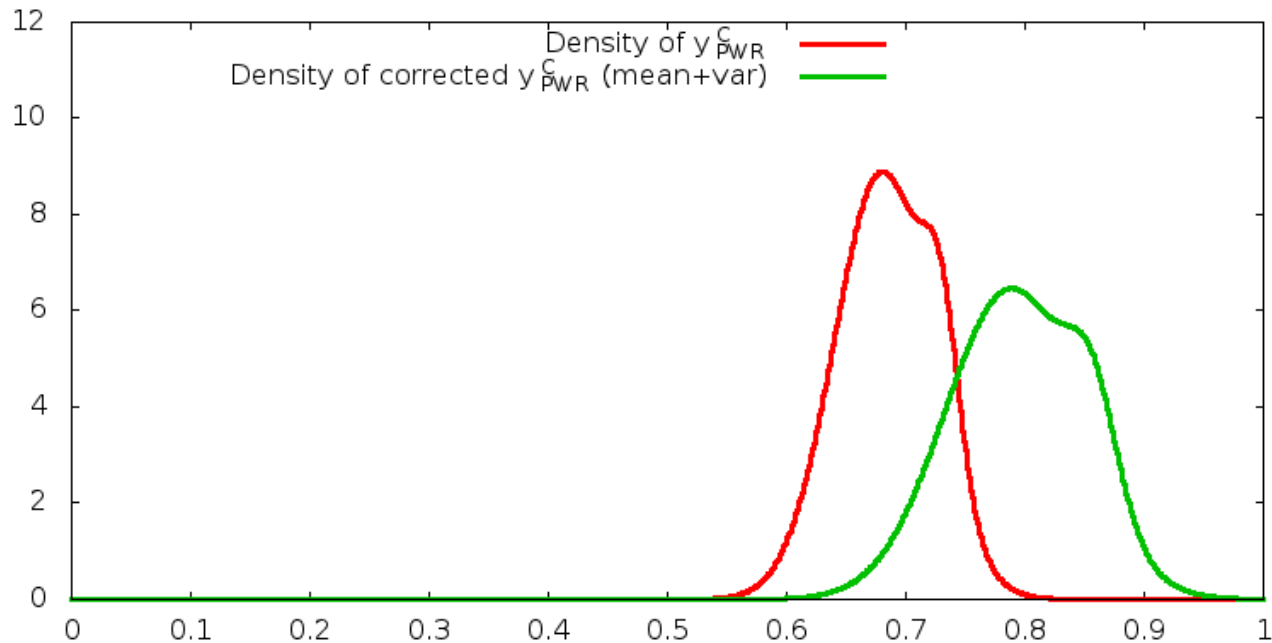
$$\mu_{\text{PWR}}^{\text{C}}(\underline{x}_{\text{PWR}}^{\text{C}}) = \arg \min_{\underline{x}_{\text{PWR}}^{\text{C}}} \left\{ \sum_{i=1}^{n_{\text{PWR}}^{\text{C}}} [y_{\text{PWR}}^{\text{C}} - \mu_{\text{PWR}}^{\text{C}}(\underline{x}_{\text{PWR}, i}^{\text{C}})]^2 \right\}$$

Step-by-step description of the procedure

- Once this term calculated, it is possible to correct each Model result with, also, the tendency, observed at test case scale, to under- / over- estimate inherent variability of the results:

$$\varphi(y_{PWR}^C) = [y_{PWR}^C - \mu_{PWR}^C] \frac{\sigma_{exp}^M}{\sigma_{exp}^C} + \mu_{PWR}^C \frac{\mu_{exp}^M}{\mu_{exp}^C}$$

- Geometrically, it results in a contraction/dilatation of the density.

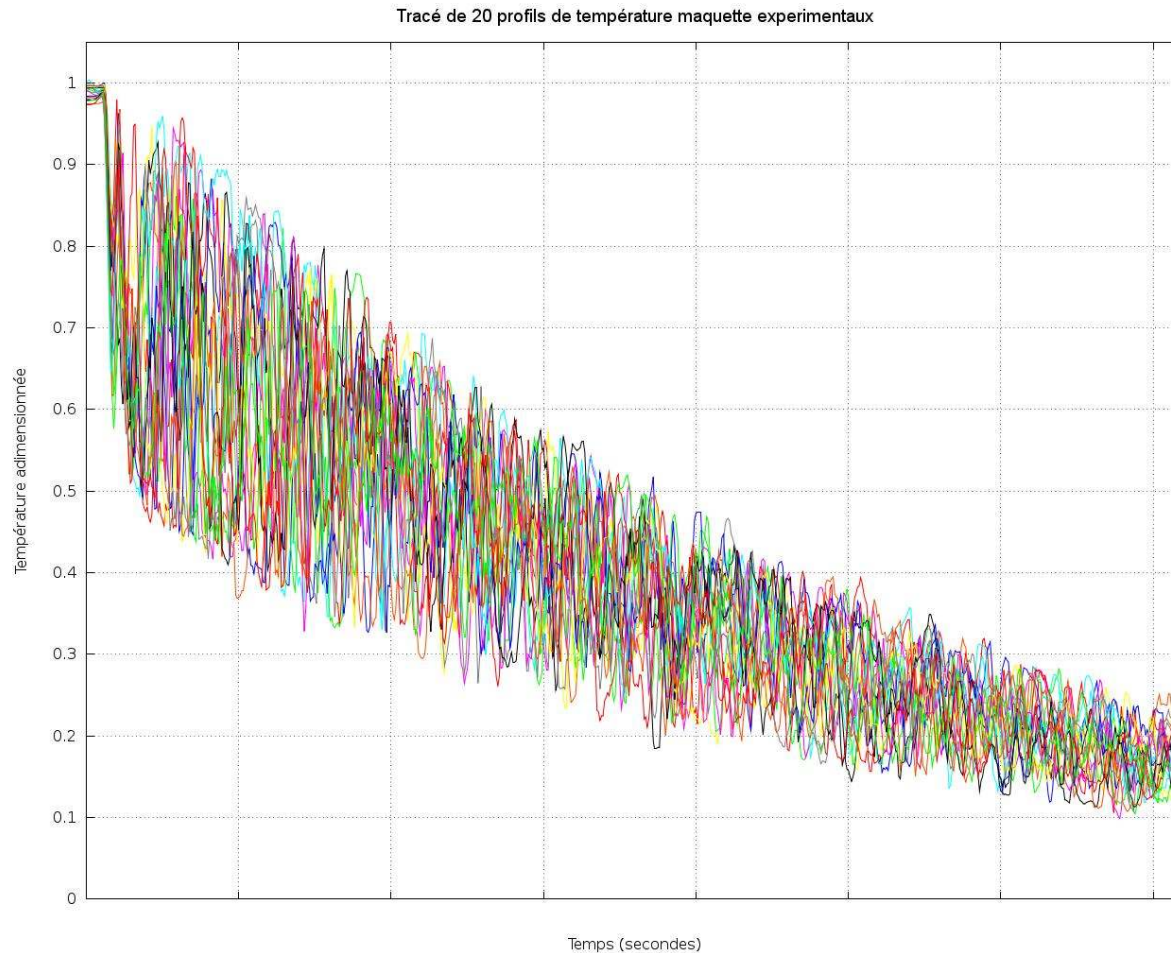


Step-by-step description of the procedure

- When dealing with results function of time, the procedure can be repeated at each time step. The same can be done for a function of space at each discrete position.
- Final results take into account:
 - Model flaws observed at test case scale ;
 - Variability due to uncertain input parameters and chaotic behavior.
- In the end, it is possible to have an estimate of the impact of each source of uncertainty (chaos and uncertain input parameters separated) on calculation results.
- Also, if transposition of errors from test case scale to industrial scale is hard to justify one can still use the piece of information: *“if my Model exhibits the same errors at industrial scale and test case scale then the impact on the results is x%”*.

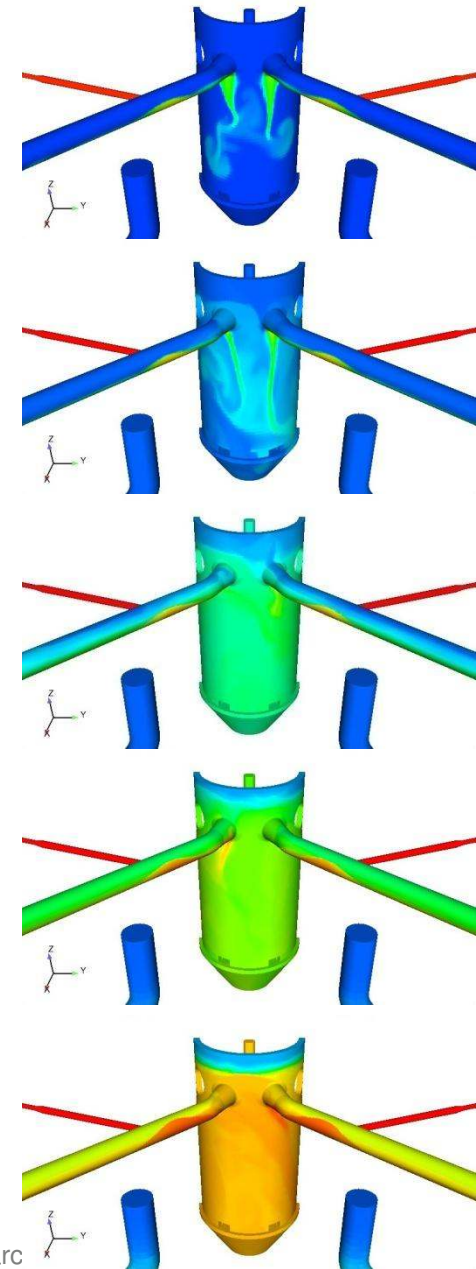
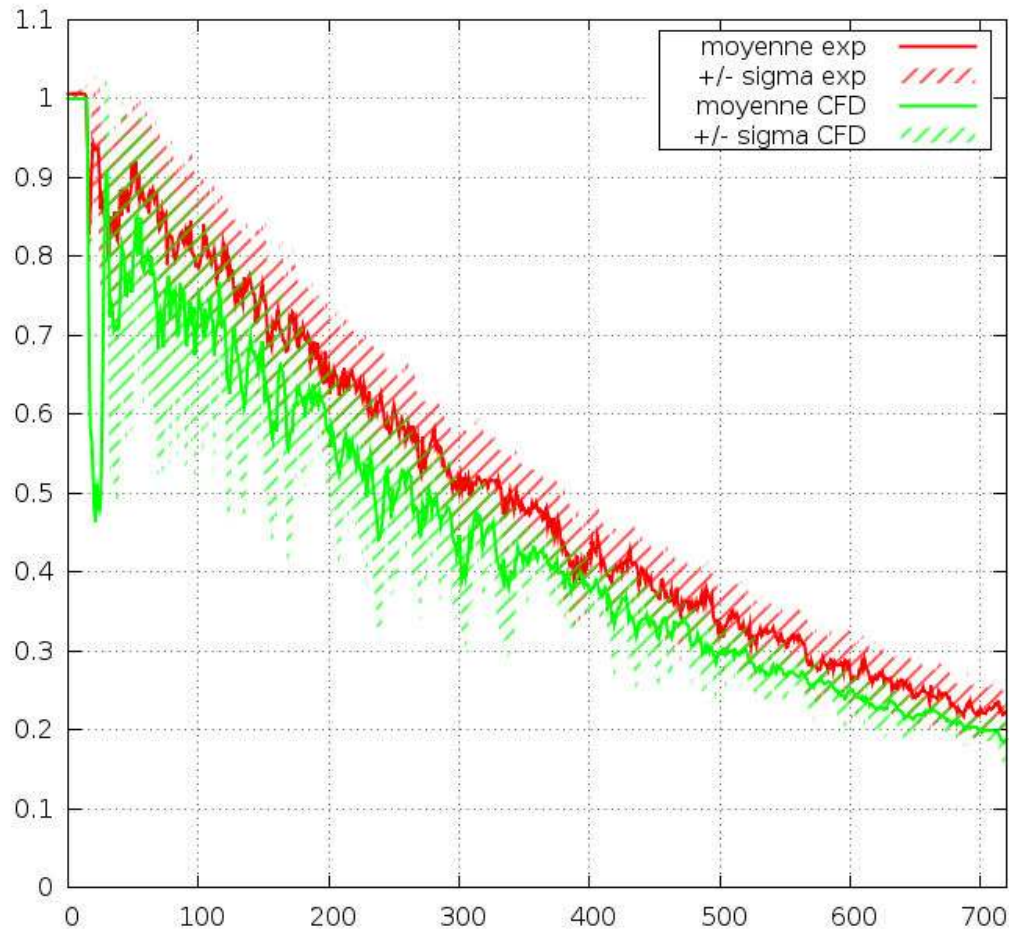
Results in an actual R&D nuclear study

- Here are 20 temperature profiles obtained at a given location for repeated experiments on HYBISCUS II:



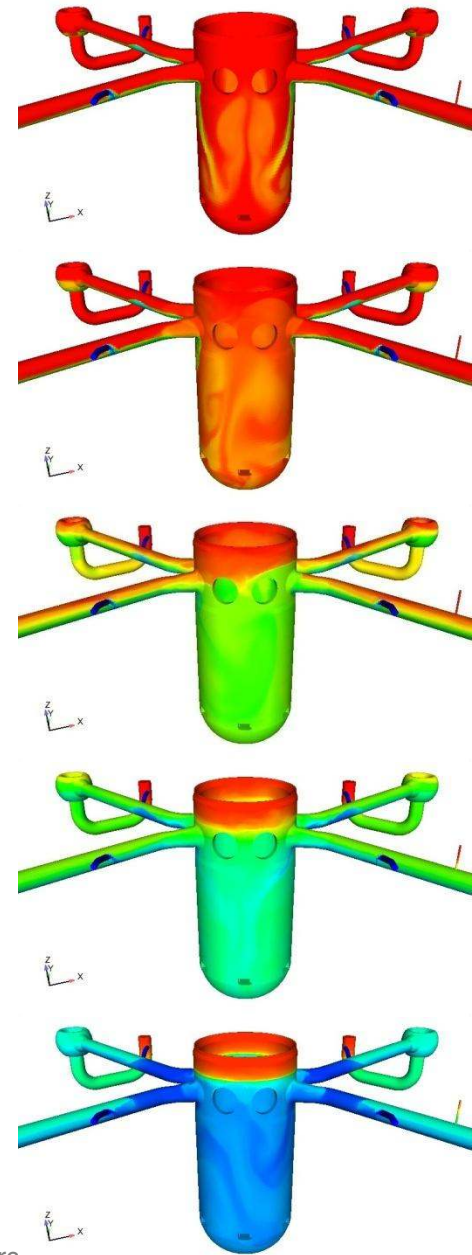
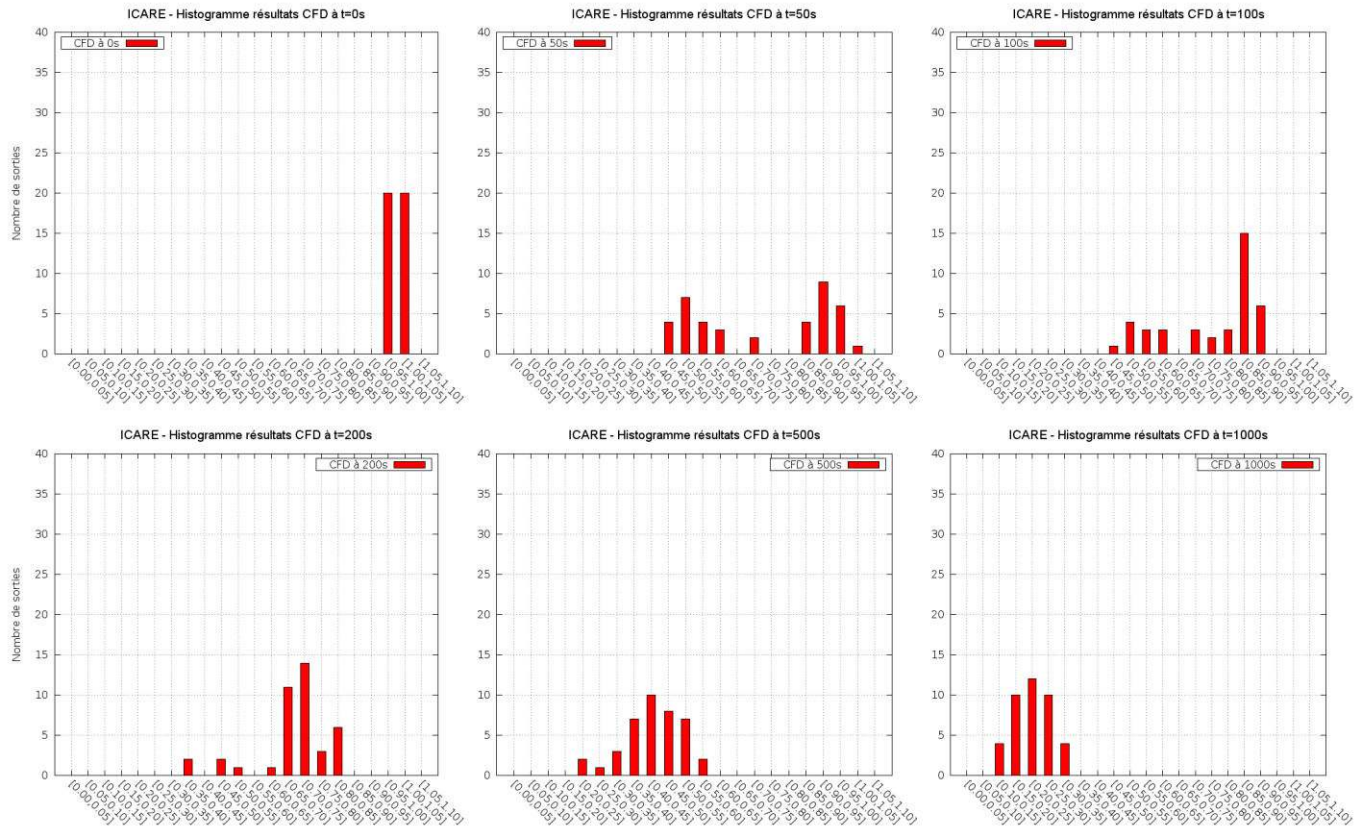
Results in an actual R&D nuclear study

- At this location, comparison with 20 CFD results by mean and variance gives:



Results in an actual R&D nuclear study

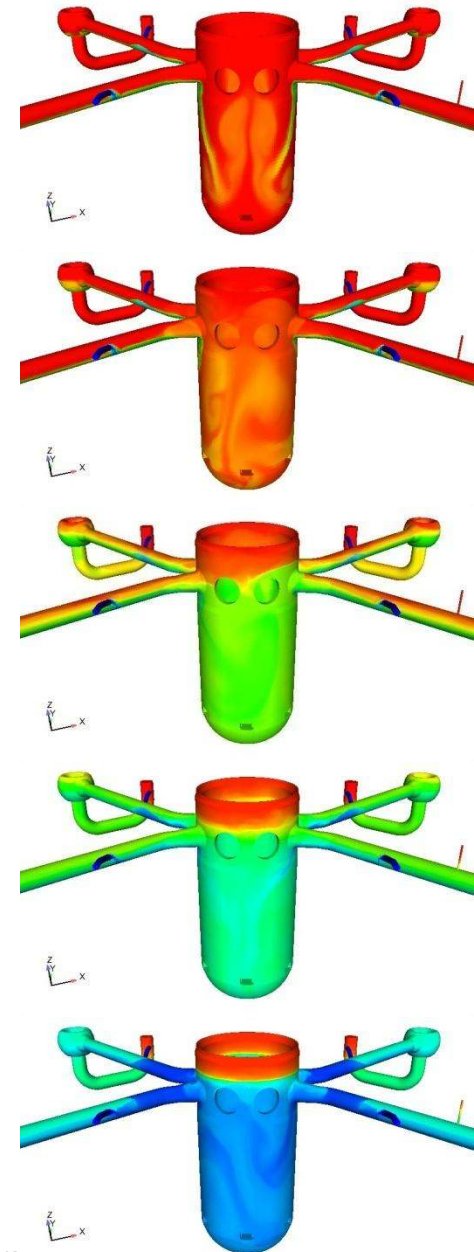
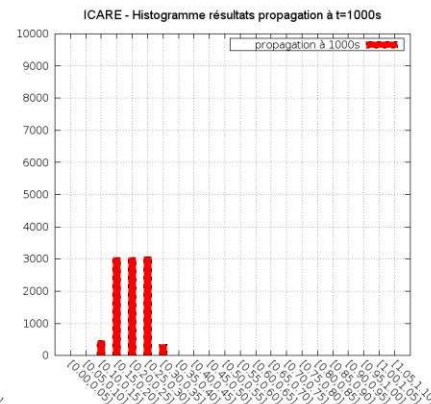
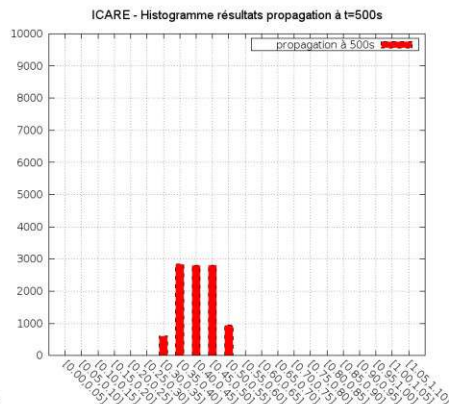
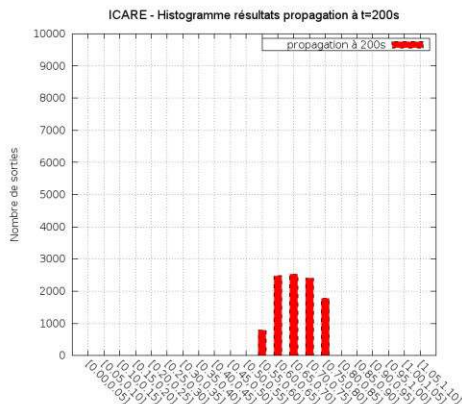
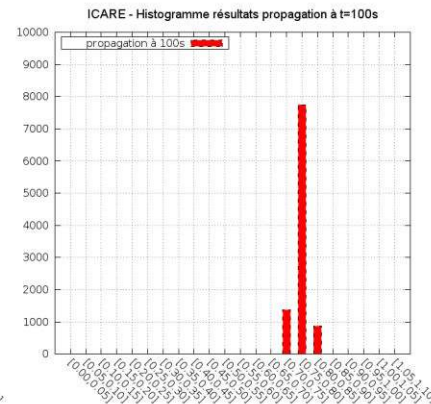
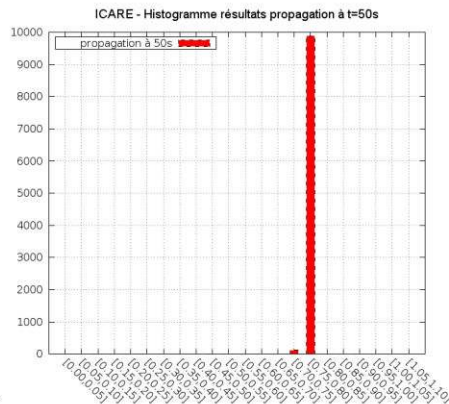
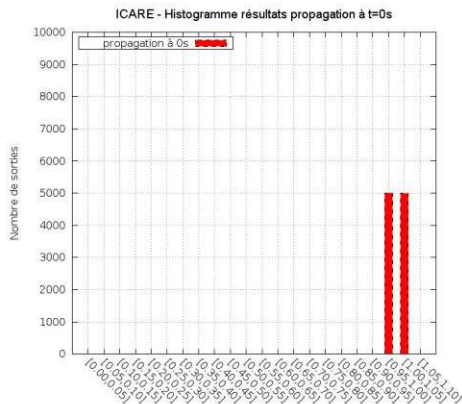
- Here are 40 CFD results (bar charts only used for visualization) at different times:



Results in an actual R&D nuclear study

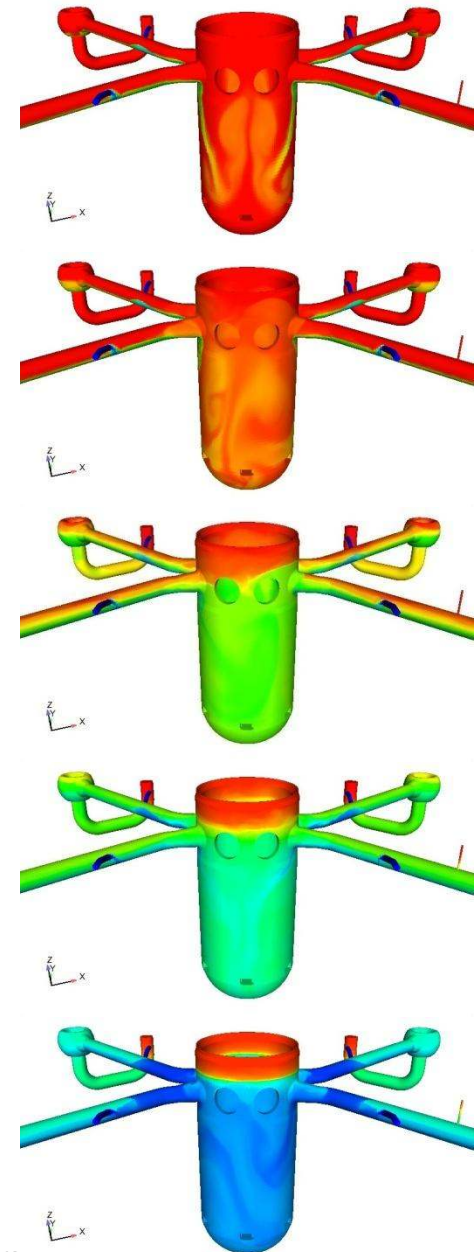
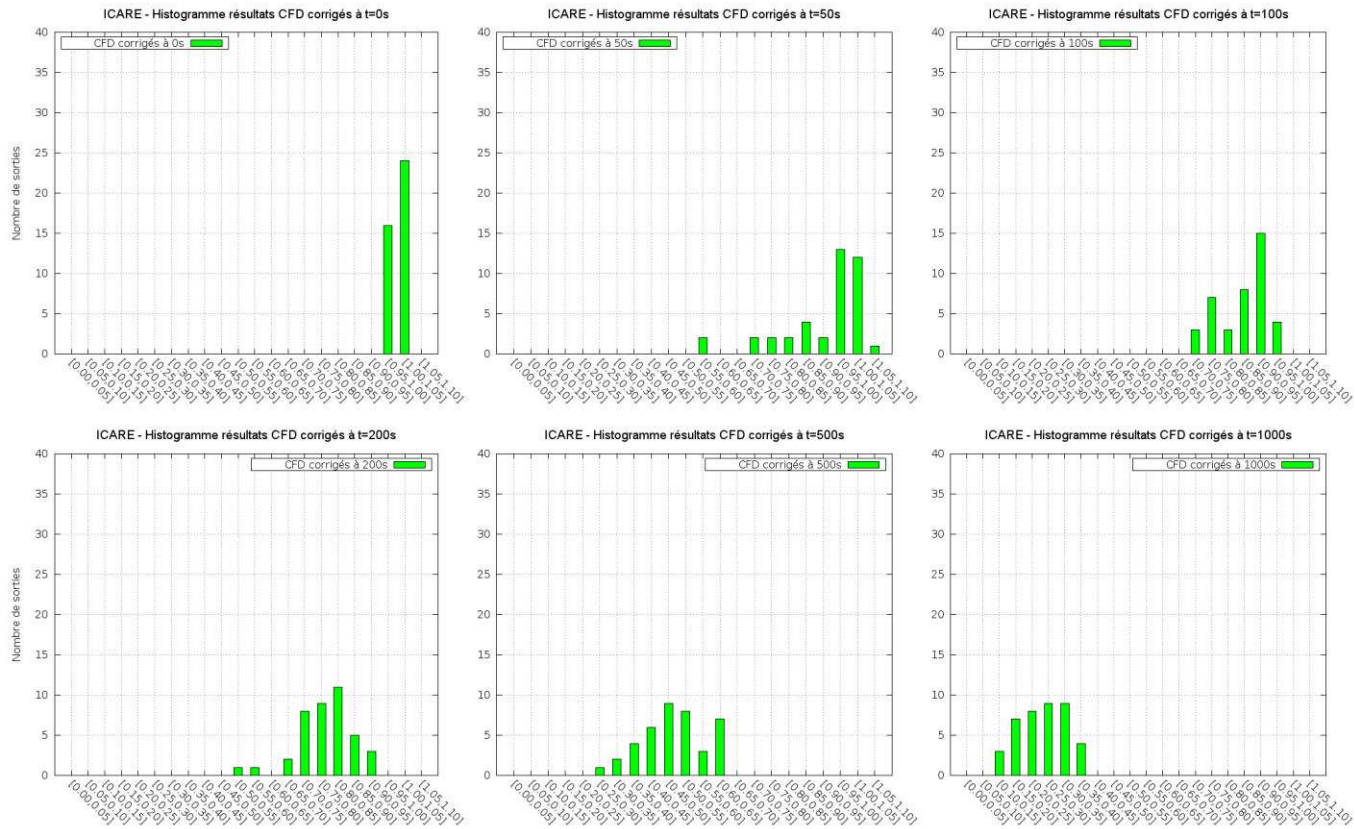
- Variance due to variability of input parameters gives following results:

$$\mu_{\text{PWR}}^C(\underline{x}_{\text{PWR}}^C) = \sum_{i=1}^{n_{\text{PWR}}^C} a_i x_i + a_0$$



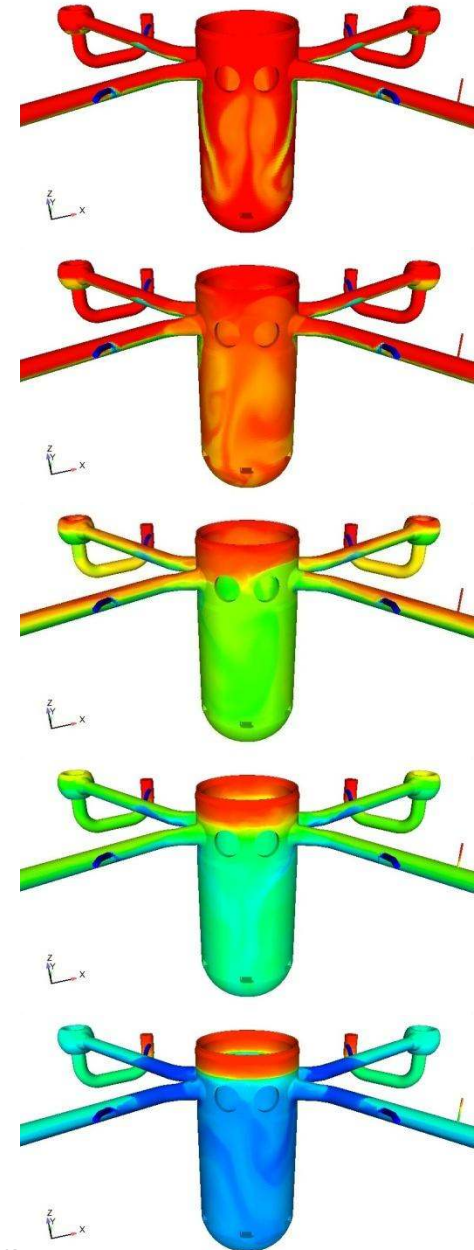
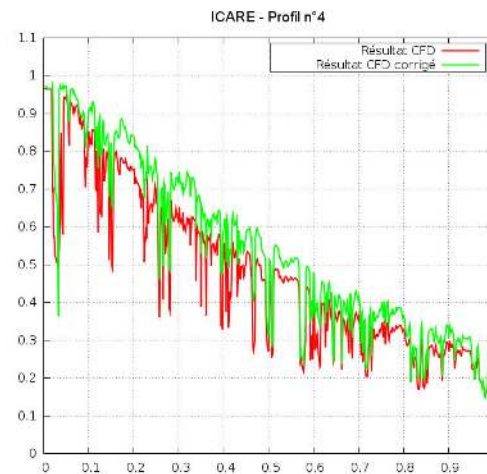
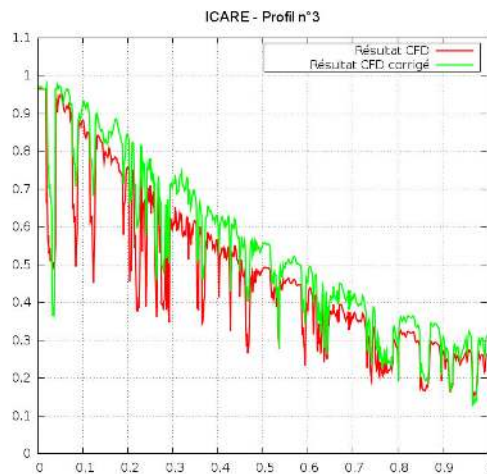
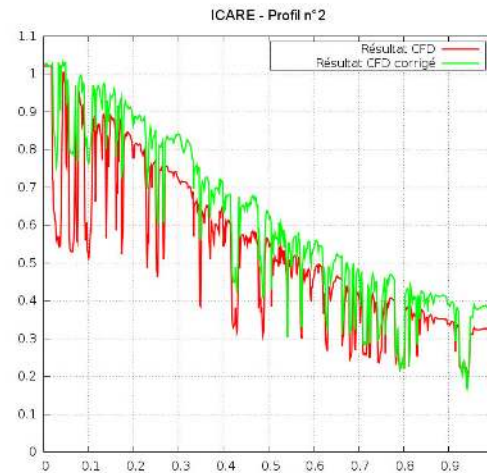
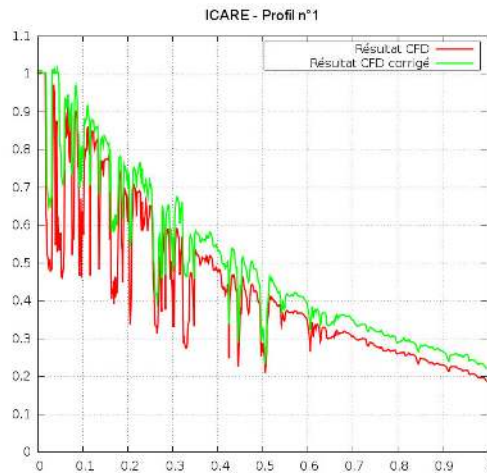
Results in an actual R&D nuclear study

- Finally, corrected 40 CFD PWR results (note densities very different from Gaussian law):



Results in an actual R&D nuclear study

- Individual (4 out of 40) corrected CFD PWR results:



Conclusions & short term prospects

- Conclusions:
 - Reasonably simple approach to deal with complex simulations.
 - Available in a verified code.
 - Recent development: estimate of uncertainties due to limited size of datasets (by bootstrap method).
- Short term prospects:
 - Use of OpenTURNS to deal with complex input uncertainties.
 - Application to other studies in nuclear domain (interest for boron dilution, hydrogen risk, ...).

Thank you